

Project: 2016-driepoot

Model: Driepoot-v14

Date: 18-07-16

STRUCTURAL ANALYSIS

PROJECT

Aerial Trapeze Truss Tripod

CLIENT

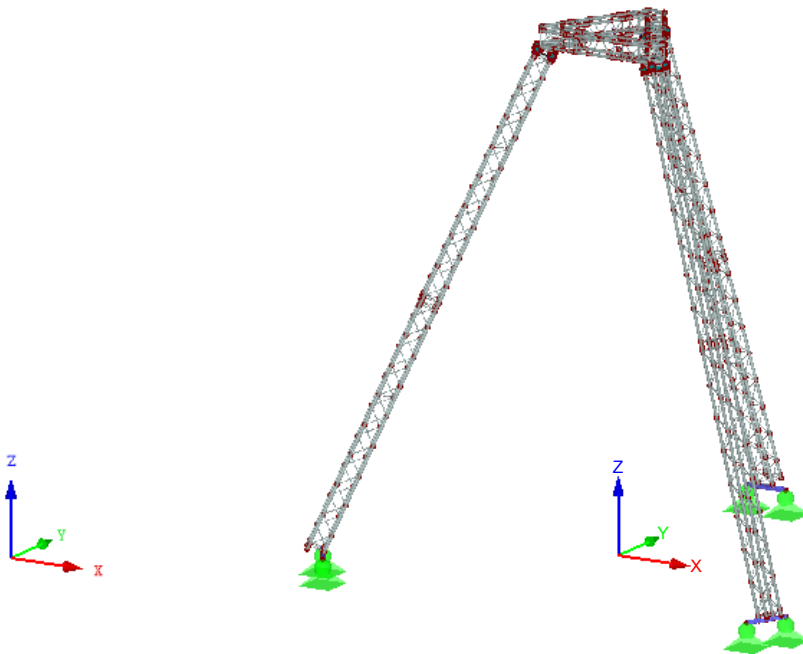
SOL'AIR

Sylvia Idelberger
Amsterdam

CREATED BY

ir. Roy Schilderman

Isometric



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■ MODEL - GENERAL DATA

	General	Model name	:	Driepoot-v14
		Project name	:	2016-driepoot
		Type of model	:	3D
		Positive direction of global axis Z	:	Upward
		Classification of load cases and combinations	:	According to Standard: EN 1990 National Annex: NEN - Netherlands

■ FE MESH SETTINGS

	General	Target length of finite elements	l_{FE}	:	15.0 mm
		Maximum distance between a node and a line to integrate it into the line	ϵ	:	0.5 mm
		Maximum number of mesh nodes (in thousands)		:	500
	Members	Number of divisions of members with cable, elastic foundation, taper, or plastic characteristic		:	10
		<input checked="" type="checkbox"/> Activate member divisions for large deformation or post-critical analysis			
		<input checked="" type="checkbox"/> Use division for members with node lying on them			
	Surfaces	Maximum ratio of FE rectangle diagonals	Δ_D	:	1.8
		Maximum out-of-plane inclination of two finite elements	α	:	0.50 °
		Shape direction of finite elements		:	Triangles and quadrangles <input checked="" type="checkbox"/> Same squares where possible

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■ CALCULATION BASE

The top section of the tripod is a one-off special product by Prolyte Netherlands. It consists of 60 deg corners with 0m75 straight parts, welded on aluminum plates to attach the H30V legs.

In the calculation a worst case slinging is applied to analyze the strenght of the top section. Normally the 3 point bridle should be attached to the upper chords of the corner sections.

In this report the following is taken into consideration:

- horizontal wind load without weight of the acrobats
- horizontal swing simultaneously with wind force for +Y (CO7) and -Y (CO8) direction
- the strength of the aluminum surfaces is analysed
- the strenght of all the members is analysed with RF_STEEL, taking the yield strenght of the aluminum in the HAZ
- in an spreadsheet a calculation is done to analyse the lifting and sliding of the construction

The EN 13814 Fairground and amusement park machinery and Structures - safety is used as a base:

- maximum allowable wind speed in service: 15 m/s
- combined wind pressure till 8m: 0.2 kN/m^2
- combined c-index: 1.2
- partial safety facror: 1.2

This results in following member loads:

- 48/3 tubes: 0.01152 kN/m
- 30/3 tubes: 0.0072 kN/m
- 18/2 tubes: 0.00432 kN/m
- 16/2 tubes: 0.00384 kN/m

■ CONCLUSIONS

The construction is strong enough to withstand wind an dynamic acrobatics.

Considering a friction coefficient of 0,6: at full wind speed in -Y direction the construction is not heavy enough to withstand the wind. A ballast of minimum 222 kg should be applied at the leg in the direction of the wind, to prevent sliding.

The construction might also be pinned to the ground.

To prevent overturning a ballast of 50 kg should be applied in the leg in the +Y direction (wind direction where it comes FROM)

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1.3 MATERIALS

Matl. No.	Modulus E [N/mm ²]	Modulus G [N/mm ²]	Poisson's Ratio ν [-]	Spec. Weight γ [kN/m ³]	Coeff. of Th. Exp. α [1/°C]	Partial Factor γ_M [-]	Material Model
1	Aluminium EN-AW 6082 T6/T651 EN 1999-1-1:2007 70000.0	27000.0	0.296	27.00	2.30E-05	1.00	Isotropic Linear Elastic
2	HDT1200M 1.0965 EN 10346:2009-03 210000.0	80769.2	0.300	78.50	1.20E-05	1.00	Isotropic Linear Elastic
3	Steel S 235 JR EN 10025-2:2004-11 210000.0	80769.2	0.300	78.50	1.20E-05	1.00	Isotropic Linear Elastic
4	grade 8 steel for bolts and pins 21000.0	10500.0	0.000	0.30	7.85E+01	1.00	Isotropic Linear Elastic

1.5 SOLIDS

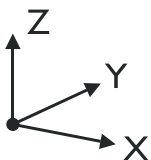
Solid No.	Solid Type	Boundary Surfaces No.	Matl. No.	Volume V [mm ³]	Weight W [kg]
1	Material	4,98,7	4	7115.5	0.00
2	Material	36,51,14	4	7115.4	0.00
3	Material	20,110,31	4	7115.5	0.00
4	Material	60,29,32	4	7115.6	0.00
5	Material	111,47,33	4	7115.2	0.00
6	Material	58,61,34	4	7115.1	0.00
7	Material	75,52,120	4	7115.1	0.00
8	Material	59,76,116	4	7115.1	0.00
9	Material	77,50,80	4	7114.7	0.00
10	Material	78,86,89	4	7114.8	0.00
11	Material	55,95,113	4	7114.7	0.00
12	Material	62,105,102	4	7114.7	0.00

1.6 OPENINGS

Opening No.	Boundary Lines No.	In Surface No.	Area A [mm ²]	Comment
1	444,443	88	200.1	
2	436,435	45	200.1	
3	428,1188	24	200.1	
4	327,326	45	200.1	
6	377,376	15	200.1	
7	336,335	6	200.1	
8	320,319	39	200.1	
9	282,281	3	200.1	
10	267,266	11	200.1	
11	386,385	13	200.1	
12	1308,369	66	200.1	
13	1253,1252	38	200.1	
14	1244,1243	114	200.1	
15	1234,1233	65	200.1	
16	370,1348	114	200.1	
17	1291,1290	109	200.1	
18	1185,1184	109	200.1	
19	1356,1355	124	200.1	
20	1340,1339	37	200.1	
21	1298,1297	122	200.1	
22	1282,1281	72	200.1	
23	1193,1192	103	200.1	
24	1176,1175	81	200.1	
25	588,587	85	200.1	
26	611,610	41	200.1	
27	1259,730	71	200.1	
28	630,629	41	200.1	
29	919,918	69	200.1	
30	901,900	69	200.1	
31	597,596	118	200.1	
32	889,739	28	200.1	
33	888,887	90	200.1	
34	740,1028	115	200.1	
35	879,878	22	200.1	
36	427,1019	123	200.1	
37	274,273	15	200.1	

1.7 NODAL SUPPORTS

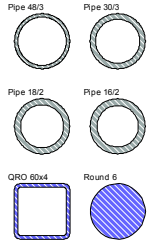
Support No.	Nodes No.	Sequen.	Rotation [°]			Column in Z	Support Conditions					
			about X	about Y	about Z		u_x	u_y	u_z	ϕ_x	ϕ_y	ϕ_z
1	3,19,396,792,1168,1184	XYZ	0.00	0.00	0.00	<input type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input checked="" type="checkbox"/>	<input type="checkbox"/>	<input type="checkbox"/>	<input checked="" type="checkbox"/>



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1.13 CROSS-SECTIONS

Section No.	Matl. No.	J [cm ⁴] A [cm ²]	I _y [cm ⁴] A _y [cm ²]		I _z [cm ⁴] A _z [cm ²]		Principal Axes α [°]	Rotation α' [°]	Overall Dimensions [mm]	
									Width b	Height h
1	Pipe 48/3 1	21.57 4.24	10.78 2.11	10.78 2.11	0.00	0.00	48.0	48.0		
2	Pipe 30/3 1	4.69 2.54	2.35 1.27	2.35 1.27	0.00	0.00	30.0	30.0		
3	Pipe 18/2 1	0.65 1.01	0.33 0.50	0.33 0.50	0.00	0.00	18.0	18.0		
4	Pipe 16/2 1	0.44 0.88	0.22 0.44	0.22 0.44	0.00	0.00	16.0	16.0		
5	QRO 60x4 EN 10210-2:2006 3	72.50 8.79	45.40 3.78	45.40 3.78	0.00	0.00	60.0	60.0		
6	Round 6 2	0.01 0.28	0.01 0.24	0.01 0.24	0.00	0.00	6.0	6.0		

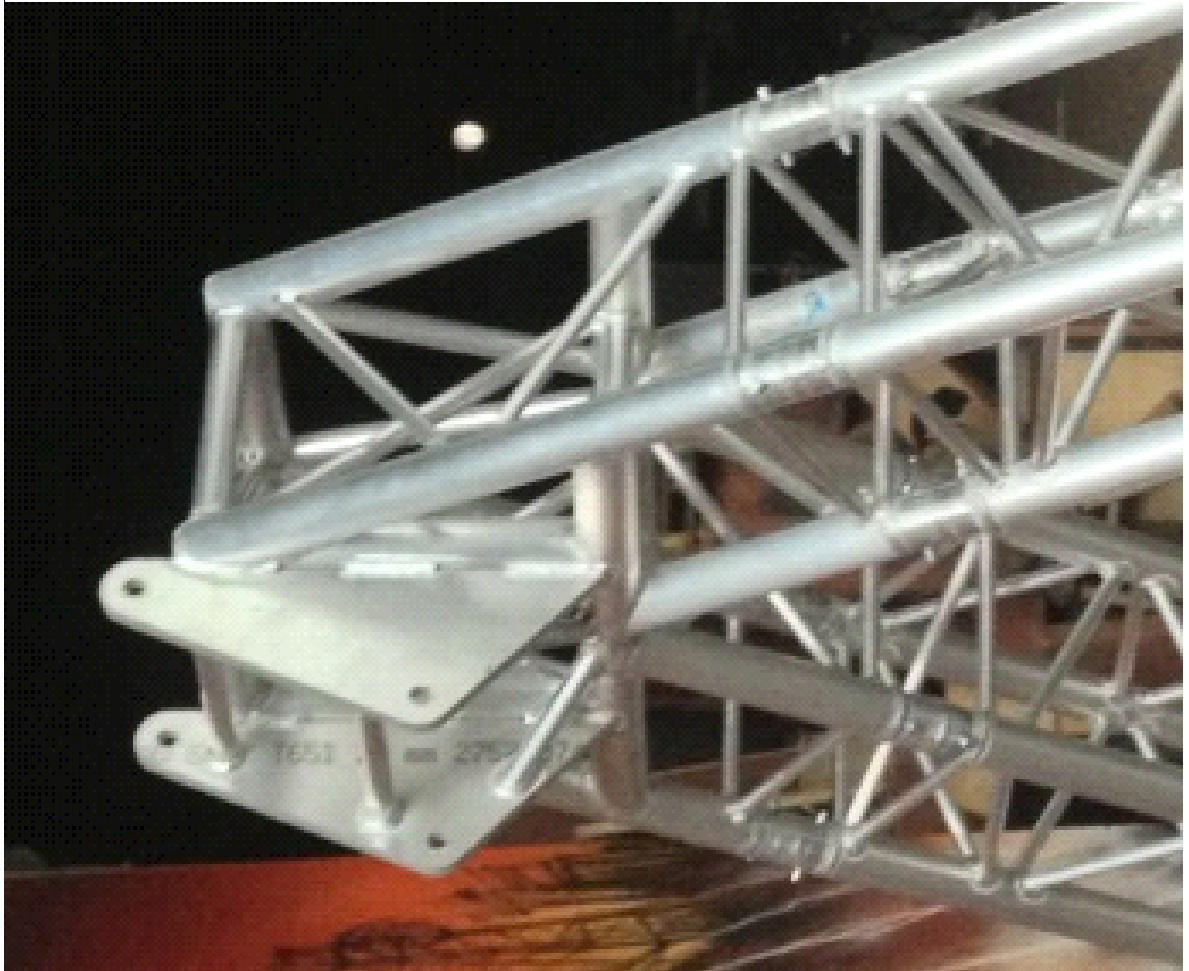
1.22 INTERSECTIONS

Inters. No.	Surfaces		Line No. Generated by Intersect.	Comment
	1st Surface No.	2nd Surface No.		
2	56	88	429	
3	24	56	414	
4	6	10	413	
5	10	39	259	
6	3	5	269	
7	5	11	258	
8	13	54	371	
9	54	66	359	
10	38	99	1261	
11	65	99	1248	
12	121	124	1363	
13	37	121	1353	
14	44	122	1311	
15	44	72	1295	
16	43	103	1205	
17	43	81	1190	
18	19	85	590	
19	19	71	733	
20	17	118	599	
21	17	28	742	
22	23	90	890	
23	23	115	1031	
24	22	87	881	
25	87	123	1022	

1.23 FE MESH REFINEMENTS

Refinem. No.	FE Mesh Refinement applied to	Nodes No.	Number Divisions	Sphere Radius [mm]	Target FE-Length [mm]		Comment
					Inner	Outer	
1	Solids	1-12		5.0			
2	Surfaces	40,68, 127-135, 148-150		10.0			
3	Surfaces	3,6,11,13, 15,22,24, 28,37-39, 41,45,65, 66,69,71, 72,81,85, 88,90,103, 109,114, 115,118, 122-124		15.0			

■ **DETAIL OF ATTACHMENT H30V LEG - TOP SECTION**



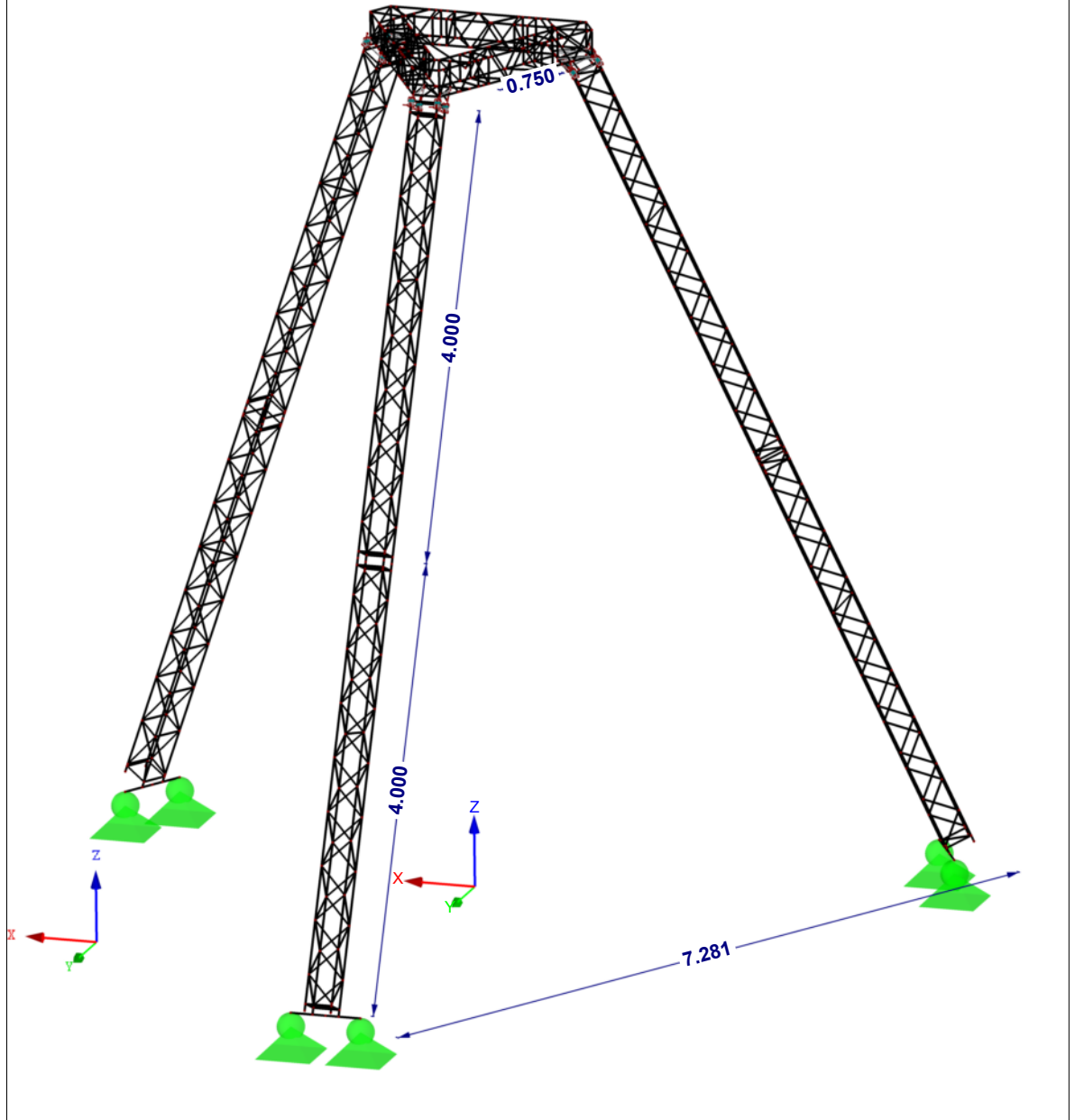
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MODEL WITH SIZES

Isometric

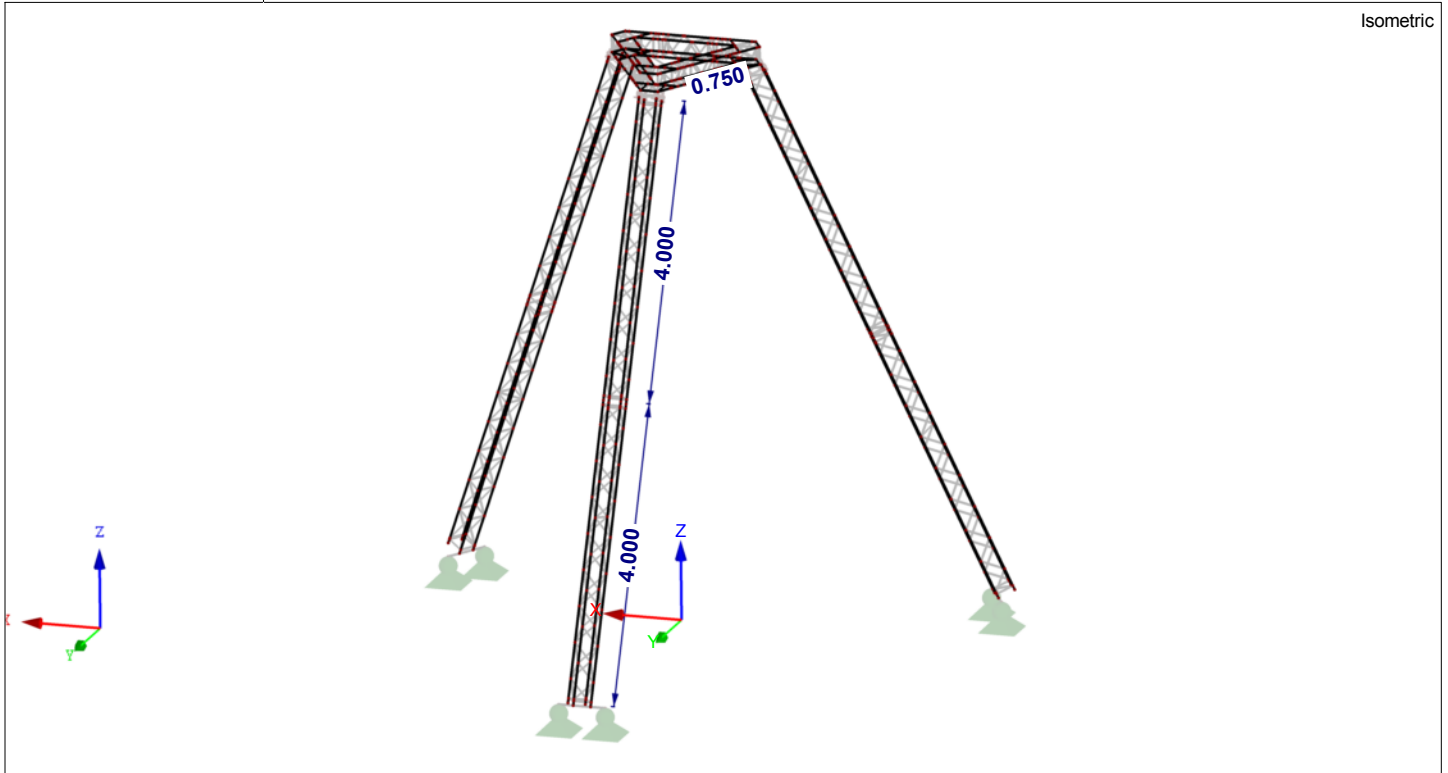


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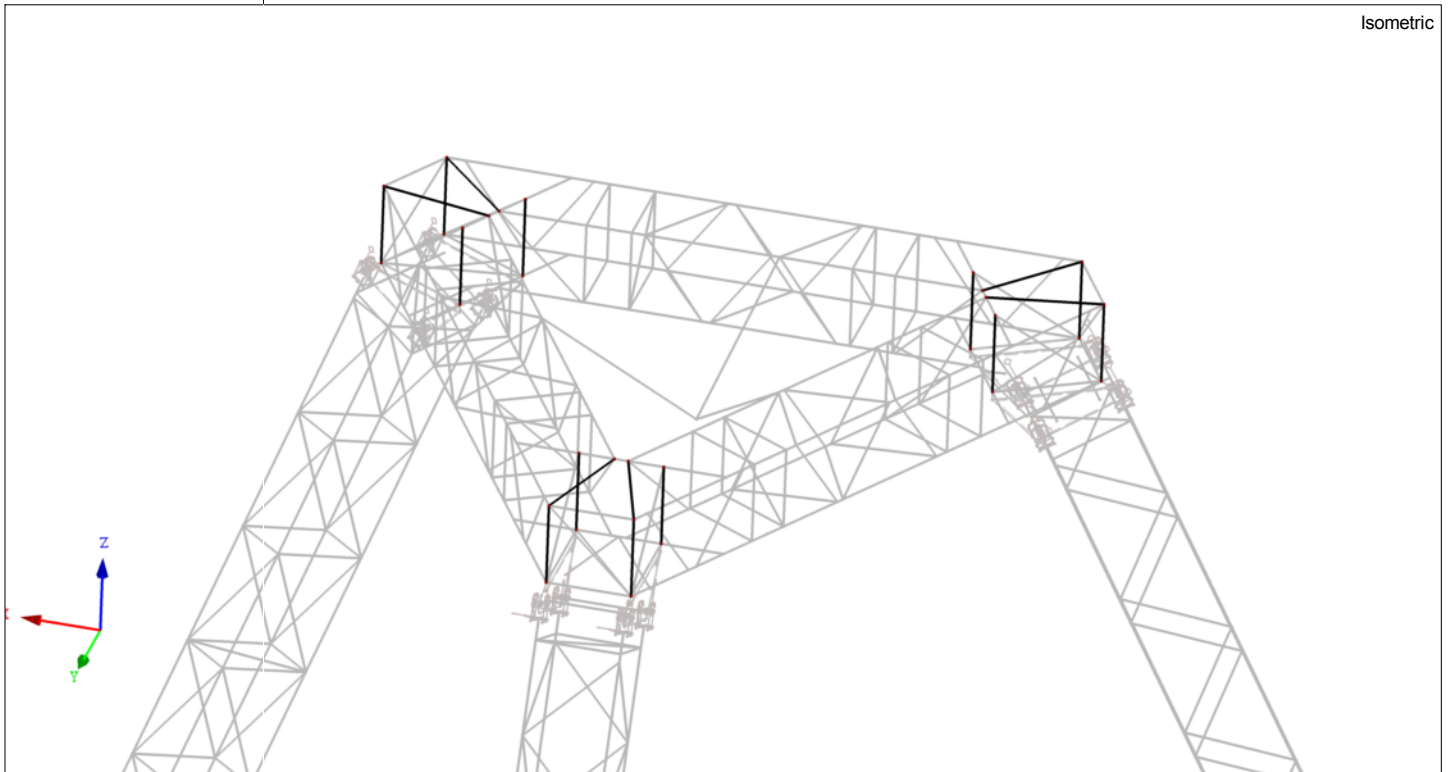
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■ **MODEL - TUBES 48 X 3**



■ **MODEL - TUBES 30/3**



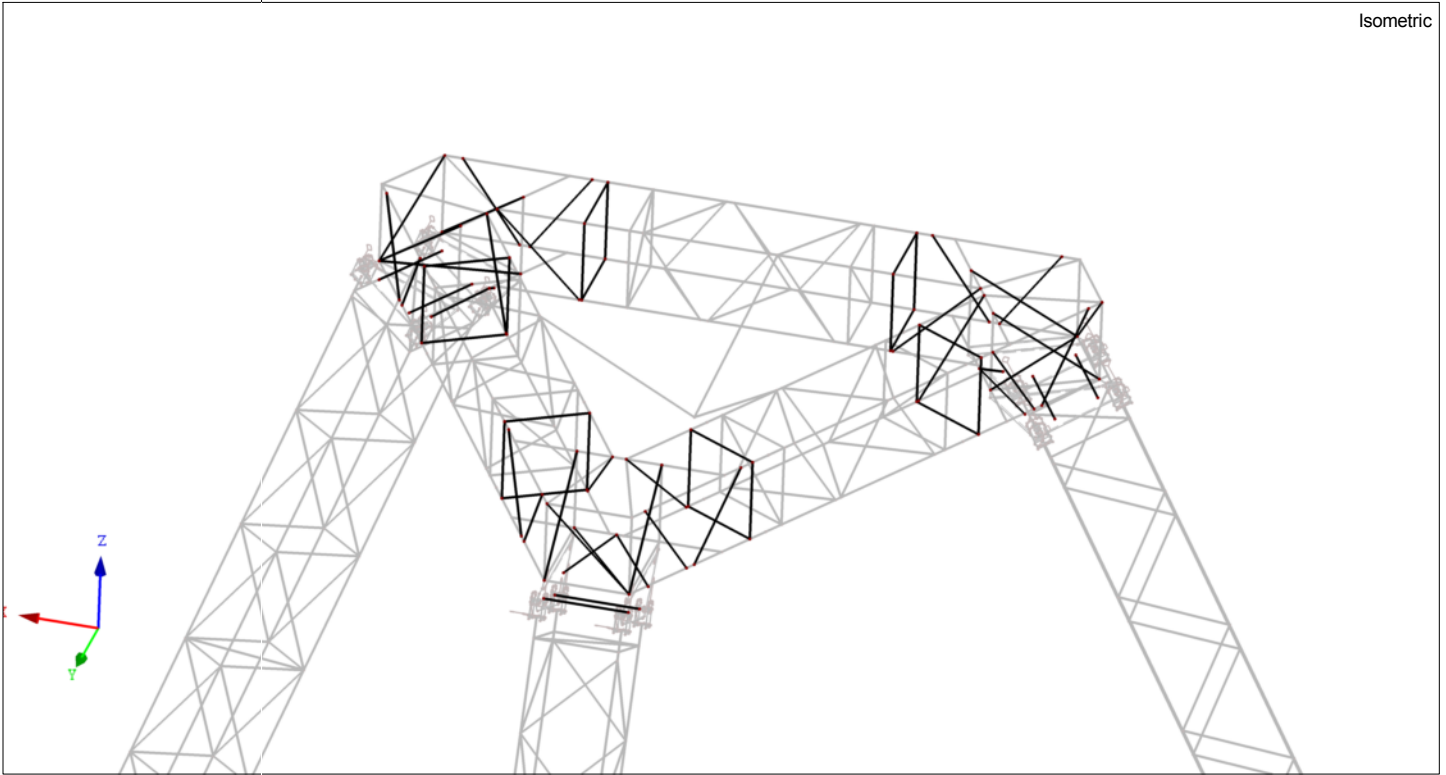
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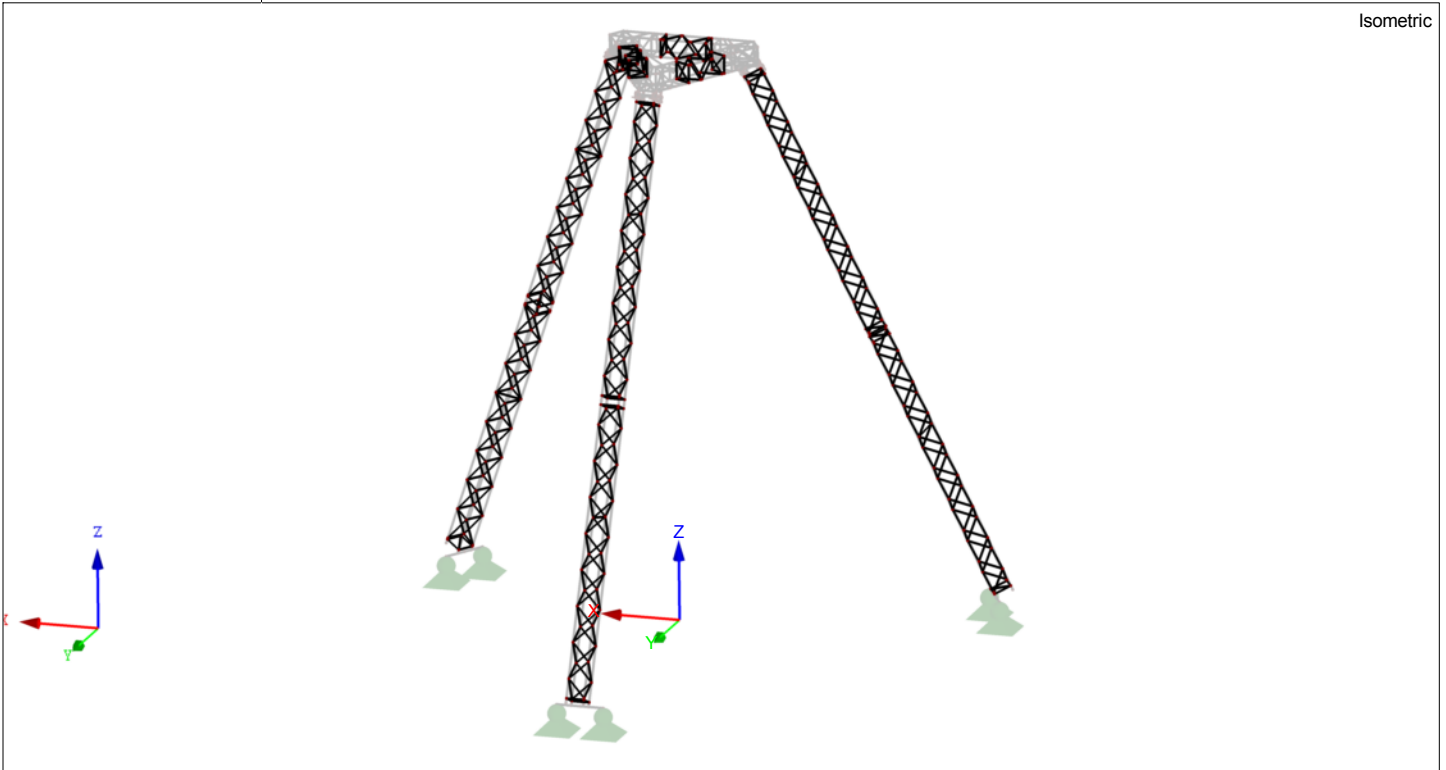
■ **MODEL - TUBES 18/2**

Isometric



■ **MODEL - TUBES 16/2**

Isometric

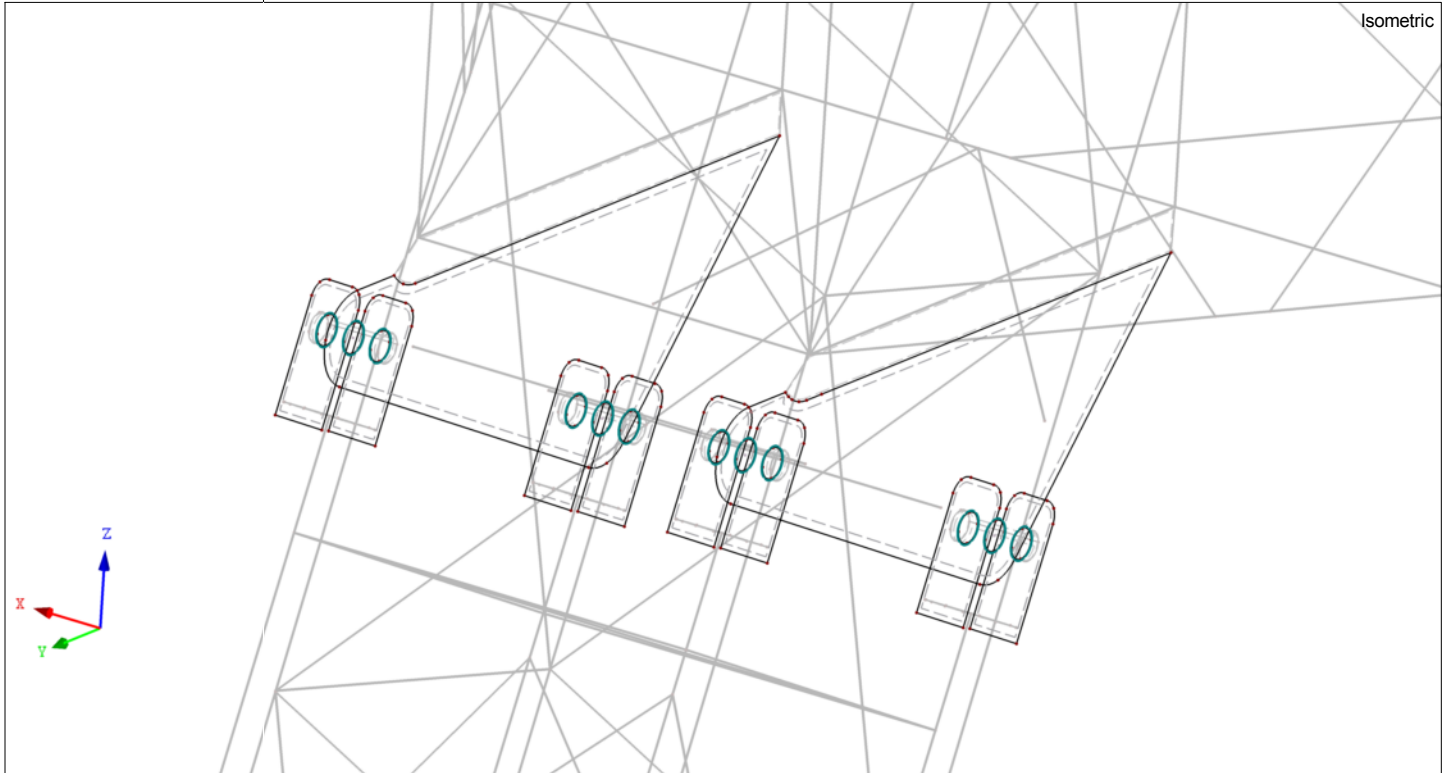


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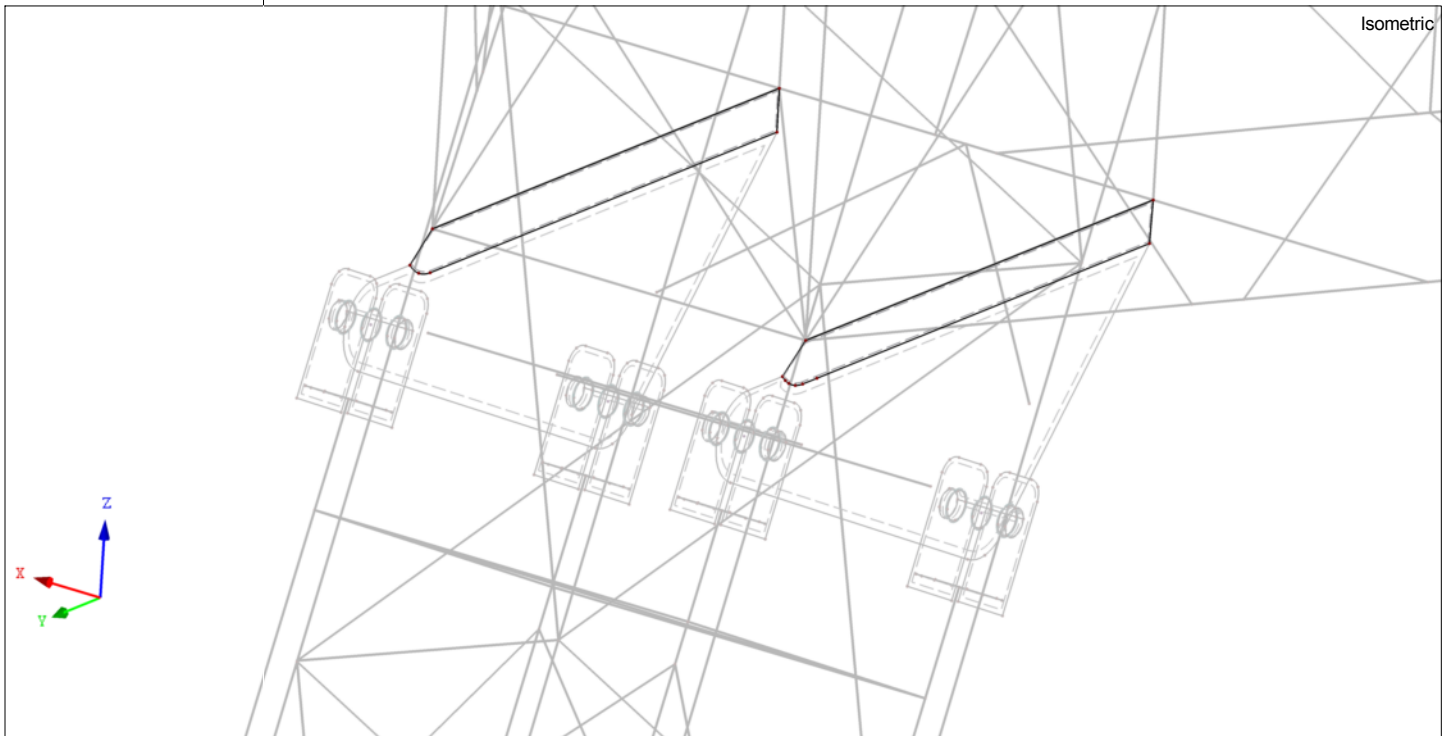
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■ MODEL - SWIVEL ATTACHMENT - 15 MM SURFACES



■ MODEL - SWIVEL ATTACHMENT - 15 MM SURFACES TO CONNECT 15MM SURFACES TO 48/3 TUBES IN THE MODEL

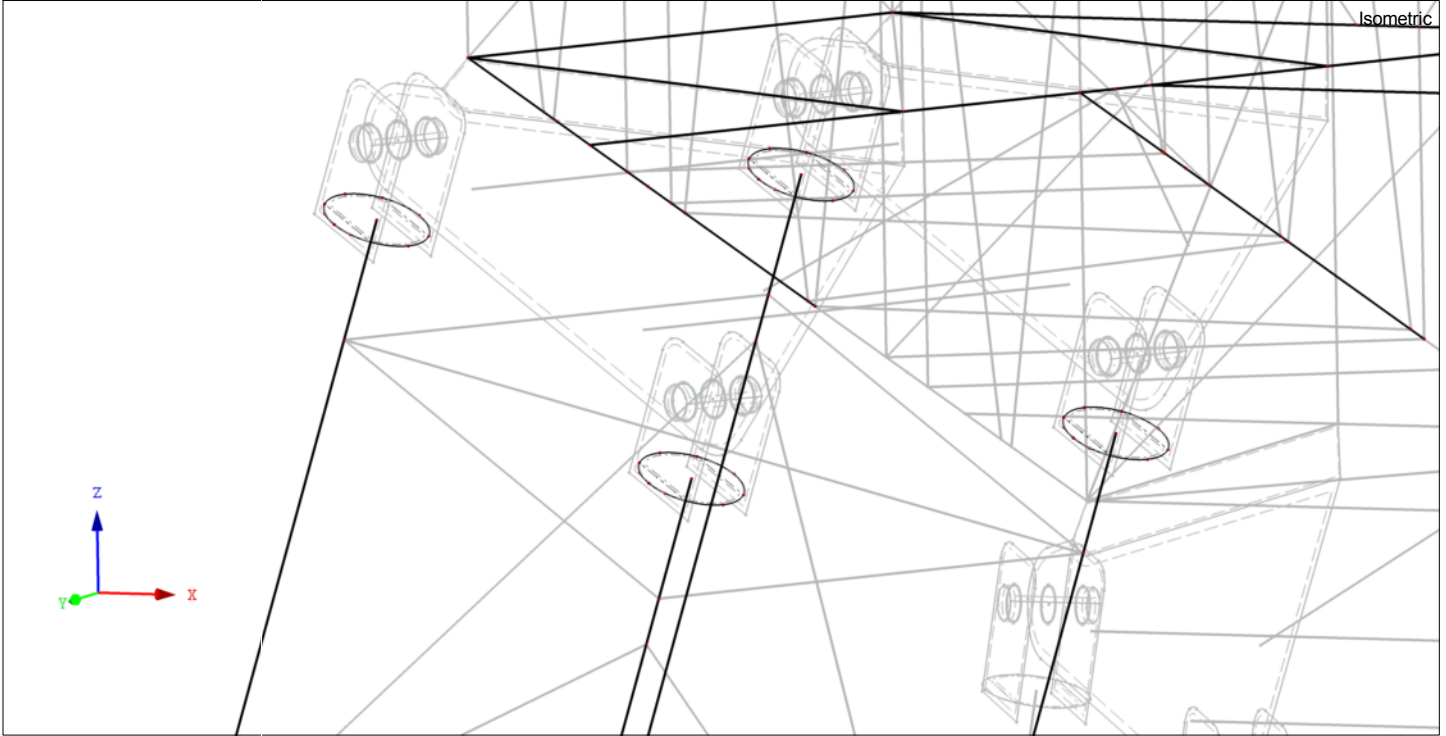


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■ **MODEL - SWIVEL ATTACHMENT - 10 MM SURFACES - TO CONNECT WIRE OF 48/3 TUBES TO HINGE FORK**



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2.1 LOAD CASES

Load Case	Load Case Description	EN 1990 NEN Action Category	Self-Weight - Factor in Direction			
			Active	X	Y	Z
LC1	Self-weight	Permanent	<input checked="" type="checkbox"/>	0.000	0.000	-1.000
LC2	Imposed load - 1 acrobat	Imposed - Category A: domestic, residential areas	<input type="checkbox"/>			
LC3	Imposed load - 1 acrobat horizontal +Y swingin	Imposed - Category A: domestic, residential areas	<input type="checkbox"/>			
LC4	Imposed load - 1 acrobat horizontal -Y swingin	Imposed - Category A: domestic, residential areas	<input type="checkbox"/>			
LC5	Imposed load - multiple acrobats	Imposed - Category A: domestic, residential areas	<input type="checkbox"/>			
LC6	Imposed load - multiple acrobats +Y swining	Imposed - Category A: domestic, residential areas	<input type="checkbox"/>			
LC7	Wind in +Y	Wind	<input type="checkbox"/>			
LC8	Wind in -Y	Wind	<input type="checkbox"/>			

2.1.1 LOAD CASES - CALCULATION PARAMETERS

Load Case	Load Case Description	Calculation Parameters	
		Method of analysis	Method for solving system of nonlinear algebraic equations
LC1	Self-weight	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC2	Imposed load - 1 acrobat	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC3	Imposed load - 1 acrobat horizontal +Y swingin	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC4	Imposed load - 1 acrobat horizontal -Y swingin	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC5	Imposed load - multiple acrobats	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC6	Imposed load - multiple acrobats +Y swining	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC7	Wind in +Y	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
LC8	Wind in -Y	Method of analysis : <input checked="" type="radio"/> Geometrically linear analysis	Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Newton-Raphson
		Activate stiffness factors of: : <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z)	: <input checked="" type="checkbox"/> Members (factor for G _J , E _{I_y} , E _{I_z} , EA, GA _y , GA _z)

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2.5 LOAD COMBINATIONS

Load Combin.	DS	Description	No.	Factor	Load Case
CO1		Characteristic Values	1	1.00	LC1 Self-weight
CO2		Design Internal Forces - 1 acrobat +Y swing	1	1.35	LC1 Self-weight
			2	4.00	LC2 Imposed load - 1 acrobat
			3	4.00	LC3 Imposed load - 1 acrobat horizontal +Y swingin
CO3		Design Internal Forces - 1 acrobat -Y swing	1	1.35	LC1 Self-weight
			2	4.00	LC2 Imposed load - 1 acrobat
			3	4.00	LC4 Imposed load - 1 acrobat horizontal -Y swingin
CO4		Design Internal Forces - multiple acrobats	1	1.35	LC1 Self-weight
			2	2.00	LC2 Imposed load - 1 acrobat
			3	2.00	LC3 Imposed load - 1 acrobat horizontal +Y swingin
CO5		internal forces - wind +Y	1	1.35	LC1 Self-weight
CO6		internal forces - wind -Y	2	1.20	LC7 Wind in +Y
			1	1.35	LC1 Self-weight
CO7		Design Internal Forces - 1 acrobat + wind +Y	2	1.20	LC8 Wind in -Y
			1	1.35	LC1 Self-weight
			2	4.00	LC2 Imposed load - 1 acrobat
CO8		Design Internal Forces - 1 acrobat + wind -Y	3	4.00	LC3 Imposed load - 1 acrobat horizontal +Y swingin
			4	1.20	LC7 Wind in +Y
			1	1.35	LC1 Self-weight
			2	4.00	LC2 Imposed load - 1 acrobat
			3	4.00	LC4 Imposed load - 1 acrobat horizontal -Y swingin
			4	1.20	LC8 Wind in -Y

2.5.2 LOAD COMBINATIONS - CALCULATION PARAMETERS

Load Combin.	Description	Calculation Parameters
CO1	Characteristic Values	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V_y and V_z <input checked="" type="checkbox"/> Moments M_y , M_z and M_T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ_M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I_y , I_z , A, A_y , A_z) <input checked="" type="checkbox"/> Members (factor for G, EI_y , EI_z , EA, GA_y , GA_z)
CO2	Design Internal Forces - 1 acrobat +Y swing	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V_y and V_z <input checked="" type="checkbox"/> Moments M_y , M_z and M_T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ_M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I_y , I_z , A, A_y , A_z) <input checked="" type="checkbox"/> Members (factor for G, EI_y , EI_z , EA, GA_y , GA_z)
CO3	Design Internal Forces - 1 acrobat -Y swing	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V_y and V_z <input checked="" type="checkbox"/> Moments M_y , M_z and M_T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ_M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I_y , I_z , A, A_y , A_z) <input checked="" type="checkbox"/> Members (factor for G, EI_y , EI_z , EA, GA_y , GA_z)
CO4	Design Internal Forces - multiple acrobats	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V_y and V_z <input checked="" type="checkbox"/> Moments M_y , M_z and M_T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ_M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I_y , I_z , A, A_y , A_z) <input checked="" type="checkbox"/> Members (factor for G, EI_y , EI_z , EA, GA_y , GA_z)
CO5	internal forces - wind +Y	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V_y and V_z <input checked="" type="checkbox"/> Moments M_y , M_z and M_T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ_M)

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2.5.2 LOAD COMBINATIONS - CALCULATION PARAMETERS

Load Combin.	Description	Calculation Parameters
		<input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z) <input checked="" type="checkbox"/> Members (factor for GJ, E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
CO6	internal forces - wind -Y	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V _y and V _z <input checked="" type="checkbox"/> Moments M _y , M _z and M _T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ _M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z) <input checked="" type="checkbox"/> Members (factor for GJ, E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
CO7	Design Internal Forces - 1 acrobat + wind +Y	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Consider favorable effects due to tension <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V _y and V _z <input checked="" type="checkbox"/> Moments M _y , M _z and M _T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ _M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z) <input checked="" type="checkbox"/> Members (factor for GJ, E _{I_y} , E _{I_z} , EA, GA _y , GA _z)
CO8	Design Internal Forces - 1 acrobat + wind -Y	Method of analysis : <input checked="" type="radio"/> Second order analysis (P-Delta) Method for solving system of nonlinear algebraic equations : <input checked="" type="radio"/> Picard Options : <input checked="" type="checkbox"/> Consider favorable effects due to tension <input checked="" type="checkbox"/> Refer internal forces to deformed system for: <input checked="" type="checkbox"/> Normal forces N <input checked="" type="checkbox"/> Shear forces V _y and V _z <input checked="" type="checkbox"/> Moments M _y , M _z and M _T Activate stiffness factors of: : <input checked="" type="checkbox"/> Materials (partial factor γ _M) <input checked="" type="checkbox"/> Cross-sections (factor for J, I _y , I _z , A, A _y , A _z) <input checked="" type="checkbox"/> Members (factor for GJ, E _{I_y} , E _{I_z} , EA, GA _y , GA _z)

2.7 RESULT COMBINATIONS

Result Combin.	Description	Loading
RC1	Design Internal Forces	CO1 or to CO8

3.1 NODAL LOADS - BY COMPONENTS - COORDINATE SYSTEM

LC2
Imposed load - 1 acrobat

LC2: Imposed load - 1 acrobat

No.	On Nodes No.	Coordinate System	Force [kN]			Moment [kNm]		
			P _x	P _y	P _z	M _x	M _y	M _z
1	594	0 Global XYZ	0.00000	0.00000	-0.80000	0.00000	0.00000	0.00000

3.1 NODAL LOADS - BY COMPONENTS - COORDINATE SYSTEM

LC3
Imposed load - 1 acrobat horizontal +Y swingin

LC3

No.	On Nodes No.	Coordinate System	Force [kN]			Moment [kNm]		
			P _x	P _y	P _z	M _x	M _y	M _z
1	594	0 Global XYZ	0.00000	0.16000	0.00000	0.00000	0.00000	0.00000

3.1 NODAL LOADS - BY COMPONENTS - COORDINATE SYSTEM

LC4
Imposed load - 1 acrobat horizontal -Y swingin

LC4

No.	On Nodes No.	Coordinate System	Force [kN]			Moment [kNm]		
			P _x	P _y	P _z	M _x	M _y	M _z
1	594	0 Global XYZ	0.00000	-0.16000	0.00000	0.00000	0.00000	0.00000

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3.1 NODAL LOADS - BY COMPONENTS COORDINATE SYSTEM

LC5: Imposed load - multiple acrobats

LC5
Imposed load - multiple acrobats

No.	On Nodes No.	Coordinate System	Force [kN]			Moment [kNm]		
			P _x	P _y	P _z	M _x	M _y	M _z
1	594	0 Global XYZ	0.00000	0.00000	-2.40000	0.00000	0.00000	0.00000

3.1 NODAL LOADS - BY COMPONENTS - COORDINATE SYSTEM

LC6

LC6
Imposed load - multiple acrobats +Y swining

No.	On Nodes No.	Coordinate System	Force [kN]			Moment [kNm]		
			P _x	P _y	P _z	M _x	M _y	M _z
1	594	0 Global XYZ	0.00000	-0.48000	0.00000	0.00000	0.00000	0.00000

3.2 MEMBER LOADS

LC7: Wind in +Y

LC7
Wind in +Y

No.	Reference to	On Members No.	Load Type	Load Distribution	Load Direction	Reference Length	Load Parameters		
							Symbol	Value	Unit
1	Members		Force	Uniform	YP	Projected Length	p	0.01152	kN/m
1, 2, 5, 8, 11-13, 15, 22-24, 28, 30, 32, 33, 38, 39, 42, 43, 46, 47, 52, 53, 56, 57, 60, 61, 66, 67, 70, 71, 74, 75, 80, 81, 84, 86, 89, 90, 95, 96, 99, 100, 103, 104, 109, 110, 112, 114, 117-119, 121, 125, 127, 130-132, 134, 138, 139, 143, 145-147, 150, 152, 156, 158-160, 163, 165, 167, 168, 173, 174, 177, 178, 181, 182, 187, 188, 191, 192, 195, 196, 201, 202, 205, 206, 209, 210, 215, 216, 219, 221, 224, 225, 230, 231, 234, 235, 238, 239, 244, 245, 247, 249, 252-254, 260, 262, 264-268, 270, 275-277, 280, 281, 284, 285, 290, 292-294, 296, 298, 300-303, 308-311, 313, 315-318, 321, 322, 324-326, 328, 333-338, 342, 344-346, 349-352, 354-356, 358, 361, 362, 364, 369, 371-378, 381, 382, 385-388, 390, 391, 397-399, 403, 404, 406, 408, 411, 412, 414-418, 424, 425, 427-429, 432, 433, 437, 438, 442-444, 446, 448, 449, 451, 453, 454, 456, 458, 459, 461, 463, 464, 466, 468, 469, 471, 473, 474, 476, 477, 479-481, 483, 485, 487, 489-492, 494, 496, 497, 499, 501, 502, 504, 506, 507, 509, 511, 512, 514, 516, 517, 519, 521, 522, 524, 525, 527, 528, 531-539, 541, 542, 552, 559, 561, 640, 641, 643, 645-649, 653-655, 659, 660, 662, 663, 665, 666, 668, 670, 671, 673, 675, 676, 678, 680, 681, 683, 685, 686, 688, 689, 691, 693, 695-698, 700, 702, 704, 706-708, 710, 711, 713, 714, 716, 718, 719, 721, 723, 724, 726, 728, 729, 731, 733, 734, 736, 738, 739, 741, 743-745, 748-751, 753-755, 761-764, 767-770, 772, 775, 777, 779, 780, 789-797, 801, 802, 805-812, 814, 819, 820, 822, 825, 827-829, 831-835, 838, 841, 842, 845-850, 855, 856, 858-860, 862, 865-868, 870, 872-875, 878, 881-883, 885, 886, 889-891, 893, 898-900, 902, 905, 907, 908, 912, 914, 916-919, 922, 925, 927, 930, 932, 933, 935, 938, 941, 942, 945, 948, 949, 952, 955, 956, 959, 962, 964, 967, 970, 971, 974, 977, 978, 981, 984, 985, 988, 991, 992, 995, 998, 999, 1002, 1005, 1006, 1009, 1012, 1013, 1016, 1019, 1021, 1022, 1024, 1026, 1028, 1029, 1031, 1036-1038, 1040, 1042, 1047, 1049, 1051-1053, 1058, 1060, 1061, 1063, 1065, 1067, 1068, 1070, 1073, 1076, 1077, 1080, 1083, 1084, 1087, 1090, 1091, 1094, 1097, 1099, 1102, 1105, 1106, 1109, 1112, 1113, 1116, 1119, 1120, 1123, 1126, 1127, 1130, 1133, 1134, 1137, 1140, 1141, 1144, 1147, 1148, 1151, 1154, 1157, 1158, 1160, 1163, 1165, 1170-1172, 1176, 1179, 1181, 1182 druck und zug; Z 2,4 kN/m ² -> 0.048 m ² /m +Y									
2	Members		Force	Uniform	YP	Projected Length	p	0.00720	kN/m
258, 278, 286, 297, 307, 329, 434, 440, 543, 642, 650, 657, 854, 876, 887, 897, 906, 924									
3	Members		Force	Uniform	YP	Projected Length	p	0.00432	kN/m
269, 271, 272, 282, 287, 288, 291, 299, 304-306, 314, 319, 320, 327, 339, 341, 343, 365, 368, 384, 405, 409, 410, 426, 431, 436, 540, 544, 553, 555, 558, 560, 639, 644, 652, 752, 760, 773, 774, 778, 799, 815, 818, 839, 840, 844, 857, 863, 864, 869, 877, 879, 880, 884, 892, 895, 896, 903, 911, 913, 915									
4	Members		Force	Uniform	YP	Projected Length	p	0.00384	kN/m
3, 4, 6, 9, 10, 14, 16, 18-21, 25, 26, 29, 31, 34-37, 40, 41, 44, 45, 48-51, 54, 55, 58, 59, 62-65, 68, 69, 72, 73, 76-79, 82, 83, 85, 87, 88, 91-94, 97, 98, 101, 102, 105-108, 111, 113, 115, 116, 120, 122-124, 126, 128, 129, 133, 135-137, 140-142, 144, 148, 149, 151, 153-155, 157, 161, 162, 164, 166, 169-172, 175, 176, 179, 180, 183-186, 189, 190, 193, 194, 197-200, 203, 204, 207, 208, 211-214, 217, 218, 220, 222, 223, 226-229, 232, 233, 236, 237, 240-243, 246, 248, 250, 251, 255-257, 259, 261, 263, 273, 274, 279, 283, 289, 312, 323, 330-332, 340, 347, 348, 353, 357, 359, 360, 363, 370, 379, 380, 383, 392, 394, 396, 400-402, 407, 419-423, 439, 441, 445, 447, 450, 452, 455, 457, 460, 462, 465, 467, 470, 472, 475, 478, 482, 484, 486, 488, 493, 495, 498, 500, 503, 505, 508, 510, 513, 515, 518, 520, 523, 526, 529, 530, 548-551, 554, 556, 557, 562-632, 634-637, 656, 658, 661, 664, 667, 669, 672, 674, 677, 679, 682, 684, 687, 689, 692, 694, 699, 701, 703, 705, 709, 712, 715, 717, 720, 722, 725, 727, 730, 732, 735, 737, 740, 742, 746, 747, 756-759, 766, 776, 781, 783, 785-788, 800, 803, 804, 813, 821, 823, 824, 826, 830, 836, 837, 843, 851-853, 861, 871, 894, 901, 904, 909, 910, 920, 921, 923, 926, 928, 929, 931, 934, 936, 937, 939, 940, 943, 944, 946, 947, 950, 951, 953, 954, 957, 958, 960, 961, 963, 965, 966, 968, 969, 972, 973, 975, 976, 979, 980, 982, 983, 986, 987, 989, 990, 993, 994, 996, 997, 1000, 1001, 1003, 1004, 1007, 1008, 1010, 1011, 1014, 1015, 1017, 1018, 1020, 1023, 1025, 1027, 1030, 1032-1035, 1039, 1041, 1043-1046, 1048, 1050, 1054-1057, 1059, 1062, 1064, 1066, 1069, 1071, 1072, 1074, 1075, 1078, 1079, 1081, 1082, 1085, 1086, 1088, 1089, 1092, 1093, 1095, 1096, 1098, 1100, 1101, 1103, 1104, 1107, 1108, 1110, 1111, 1114, 1115, 1117, 1118, 1121, 1122, 1124, 1125, 1128, 1129, 1131, 1132, 1135, 1136, 1138, 1139, 1142, 1143, 1145, 1146, 1149, 1150, 1152, 1153, 1156, 1159, 1161, 1162, 1164, 1166, 1168, 1169, 1173, 1174, 1177, 1178, 1180									

3.2 MEMBER LOADS

LC8: Wind in -Y

LC8
Wind in -Y

No.	Reference to	On Members No.	Load Type	Load Distribution	Load Direction	Reference Length	Load Parameters		
							Symbol	Value	Unit
1	Members		Force	Uniform	YP	Projected Length	p	-0.01152	kN/m
1, 2, 5, 8, 11-13, 15, 22-24, 28, 30, 32, 33, 38, 39, 42, 43, 46, 47, 52, 53, 56, 57, 60, 61, 66, 67, 70, 71, 74, 75, 80, 81, 84, 86, 89, 90, 95, 96, 99, 100, 103, 104, 109, 110, 112, 114, 117-119, 121, 125, 127, 130-132, 134, 138, 139, 143, 145-147, 150, 152, 156, 158-160, 163, 165, 167, 168, 173, 174, 177, 178, 181, 182, 187, 188, 191, 192, 195, 196, 201, 202, 205, 206, 209, 210, 215, 216, 219, 221, 224, 225, 230, 231, 234, 235, 238, 239, 244, 245, 247, 249, 252-254, 260, 262, 264-268, 270, 275-277, 280, 281, 284, 285, 290, 292-294, 296, 298, 300-303, 308-311, 313, 315-318, 321, 322, 324-326, 328, 333-338, 342, 344-346, 349-352, 354-356, 358, 361, 362, 364, 369, 371-378, 381, 382, 385-388, 390, 391, 397-399, 403, 404, 406, 408, 411, 412, 414-418, 424, 425, 427-429, 432, 433, 437, 438, 442-444, 446, 448, 449, 451, 453, 454, 456, 458, 459, 461, 463, 464, 466, 468, 469, 471, 473, 474, 476, 477, 479-481, 483, 485, 487, 489-492, 494, 496, 497, 499, 501, 502, 504, 506, 507, 509, 511, 512, 514, 516, 517, 519, 521, 522, 524, 525, 527, 528, 531-539, 541, 542, 552, 559, 561, 640, 641, 643, 645-649, 653-655, 659, 660, 662, 663, 665, 666, 668, 670, 671, 673, 675, 676, 678, 680, 681, 683, 685, 686, 688, 689, 691, 693, 695-698, 700, 702, 704, 706-708, 710, 7									

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3.2 MEMBER LOADS

LC8: Wind in -Y

No.	Reference to	On Members No.	Load Type	Load Distribution	Load Direction	Reference Length	Load Parameters		
							Symbol	Value	Unit
2	711,713,714,716,718,719,721,723,724,726,728,729,731,733,734,736,738,739,741,743-745,748-751,753-755,761-764,767-770,772,775,777,779,780,789-797,801,802,805-812,814,819,820,822,825,827-829,831-835,838,841,842,845-850,855,856,858-860,862,865-868,870,872-875,878,881-883,885,886,889-891,893,898-900,902,905,907,908,912,914,916-919,922,925,927,930,932,933,935,938,941,942,945,948,949,952,955,956,959,962,964,967,970,971,974,977,978,981,984,985,988,991,992,995,998,999,1002,1005,1006,1009,1012,1013,1016,1019,1021,1022,1024,1026,1028,1029,1031,1036-1038,1040,1042,1047,1049,1051-1053,1058,1060,1061,1063,1065,1067,1068,1070,1073,1076,1077,1080,1083,1084,1087,1090,1091,1094,1097,1099,1102,1105,1106,1109,1112,1113,1116,1119,1120,1123,1126,1127,1130,1133,1134,1137,1140,1141,1144,1147,1148,1151,1154,1157,1158,1160,1163,1165,1170-1172,1176,1179,1181,1182	Force	Uniform	YP	Projected Length	p	-0.00720	kN/m	
3	258,278,286,297,307,329,434,440,543,642,650,657,854,876,887,897,906,924	Force	Uniform	YP	Projected Length	p	-0.00432	kN/m	
4	269,271,272,282,287,288,291,299,304-306,314,319,320,327,339,341,343,365,368,384,405,409,410,426,431,436,540,544,553,555,558,560,639,644,652,752,760,773,774,778,799,815,818,839,840,844,857,863,864,869,877,879,880,884,892,895,896,903,911,913,915	Force	Uniform	YP	Projected Length	p	-0.00384	kN/m	
3,4,6,9,10,14,16,18-21,25,26,29,31,34-37,40,41,44,45,48-51,54,55,58,59,62-65,68,69,72,73,76-79,82,83,85,87,88,91-94,97,98,101,102,105-108,111,113,115,116,120,122-124,126,128,129,133,135-137,140-142,144,148,149,151,153-155,157,161,162,164,166,169-172,175,176,179,180,183-186,189,190,193,194,197-200,203,204,207,208,211-214,217,218,220,222,223,226-229,232,233,236,237,240-243,246,248,250,251,255-257,259,261,263,273,274,279,283,289,312,323,330-332,340,347,348,353,357,359,360,363,370,379,380,383,392,394,396,400-402,407,419-423,439,441,445,447,450,452,455,457,460,462,465,467,470,472,475,478,482,484,486,488,493,495,498,500,503,505,508,510,513,515,518,520,523,526,529,530,548-551,554,556,557,562-632,634-637,656,658,661,664,667,669,672,674,677,679,682,684,687,689,692,694,699,701,703,705,709,712,715,717,720,722,725,727,730,732,735,737,740,742,746,747,756-759,766,776,781,783,785-788,800,803,804,813,821,823,824,826,830,836,837,843,851-853,861,871,894,901,904,909,910,920,921,923,926,928,929,931,934,936,937,939,940,943,944,946,947,950,951,953,954,957,958,960,961,963,965,966,968,969,972,973,975,976,979,980,982,983,986,987,989,990,993,994,996,997,1000,1001,1003,1004,1007,1008,1010,1011,1014,1015,1017,1018,1020,1023,1025,1027,1030,1032-1035,1039,1041,1043-1046,1048,1050,1054-1057,1059,1062,1064,1066,1069,1071,1072,1074,1075,1078,1079,1081,1082,1085,1086,1088,1089,1092,1093,1095,1096,1098,1100,1101,1103,1104,1107,1108,1110,1111,1114,1115,1117,1118,1121,1122,1124,1125,1128,1129,1131,1132,1135,1136,1138,1139,1142,1143,1145,1146,1149,1150,1152,1153,1156,1159,1161,1162,1164,1166,1168,1169,1173,1174,1177,1178,1180									

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4.0 RESULTS - SUMMARY

Description	Value	Unit	Comment
LC1 - Self-weight			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	0.00	kN	
Sum of support reactions in Y	0.00	kN	
Sum of loads in Z	-2.13	kN	
Sum of support reactions in Z	-2.13	kN	
Resultant of reactions about X	-0.00007	kNm	Deviation 0.00%
Resultant of reactions about Y	0.00000	kNm	At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm)
Resultant of reactions about Z	0.00000	kNm	At center of gravity of model
Max. displacement in X	0.4	mm	Member No. 117, x: 46.7 mm
Max. displacement in Y	-0.4	mm	Member No. 708, x: 40.0 mm
Max. displacement in Z	-0.2	mm	Member No. 1035, x: 225.7 mm
Max. vector displacement	0.5	mm	Member No. 701, x: 143.4 mm
Max. rotation about X	0.3	mmrad	FE Node No. 1253 (X: 751.7, Y: -559.2, Z: 7382.5 mm)
Max. rotation about Y	0.3	mmrad	Member No. 7, x: 200.0 mm
Max. rotation about Z	-0.1	mmrad	FE Node No. 1680 (X: -754.4, Y: -566.3, Z: 7367.7 mm)
Method of analysis	Linear		Geometrically linear analysis
Reduction of stiffness			Cross-sections, Members, Surfaces
Number of load increments	1		
Number of iterations	1		
LC2 - Imposed load - 1 acrobat			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	0.00	kN	
Sum of support reactions in Y	0.00	kN	
Sum of loads in Z	-0.80	kN	
Sum of support reactions in Z	-0.80	kN	
Resultant of reactions about X	0.00000	kNm	Deviation 0.00%
Resultant of reactions about Y	0.00000	kNm	At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm)
Resultant of reactions about Z	0.00000	kNm	At center of gravity of model
Max. displacement in X	0.1	mm	Member No. 1049, x: 130.9 mm
Max. displacement in Y	0.1	mm	Member No. 714, x: 480.0 mm
Max. displacement in Z	-0.3	mm	Member No. 765, x: 0.0 mm
Max. vector displacement	0.3	mm	Member No. 765, x: 0.0 mm
Max. rotation about X	-0.6	mmrad	Member No. 545, x: 315.0 mm
Max. rotation about Y	-0.6	mmrad	Member No. 765, x: 315.0 mm
Max. rotation about Z	0.3	mmrad	Member No. 382, x: 46.7 mm
Method of analysis	Linear		Geometrically linear analysis
Reduction of stiffness			Cross-sections, Members, Surfaces
Number of load increments	1		
Number of iterations	1		
LC3 - Imposed load - 1 acrobat horizontal +Y swingin			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	0.16	kN	
Sum of support reactions in Y	0.16	kN	Deviation 0.00%
Sum of loads in Z	0.00	kN	
Sum of support reactions in Z	0.00	kN	
Resultant of reactions about X	-0.47377	kNm	At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm)
Resultant of reactions about Y	0.00000	kNm	At center of gravity of model
Resultant of reactions about Z	0.00000	kNm	At center of gravity of model
Max. displacement in X	0.1	mm	Member No. 124, x: 338.5 mm
Max. displacement in Y	0.7	mm	Member No. 765, x: 0.0 mm
Max. displacement in Z	0.3	mm	Member No. 678, x: 425.5 mm
Max. vector displacement	0.7	mm	Member No. 461, x: 265.9 mm
Max. rotation about X	0.4	mmrad	Member No. 430, x: 52.5 mm
Max. rotation about Y	0.2	mmrad	FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	0.2	mmrad	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Method of analysis	Linear		Geometrically linear analysis
Reduction of stiffness			Cross-sections, Members, Surfaces
Number of load increments	1		
Number of iterations	1		
LC4 - Imposed load - 1 acrobat horizontal -Y swingin			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	-0.16	kN	
Sum of support reactions in Y	-0.16	kN	Deviation 0.00%
Sum of loads in Z	0.00	kN	
Sum of support reactions in Z	0.00	kN	
Resultant of reactions about X	0.47377	kNm	At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm)
Resultant of reactions about Y	0.00000	kNm	At center of gravity of model
Resultant of reactions about Z	0.00000	kNm	At center of gravity of model
Max. displacement in X	-0.1	mm	Member No. 124, x: 338.5 mm
Max. displacement in Y	-0.7	mm	Member No. 765, x: 0.0 mm
Max. displacement in Z	-0.3	mm	Member No. 678, x: 425.5 mm
Max. vector displacement	0.7	mm	Member No. 461, x: 265.9 mm
Max. rotation about X	-0.4	mmrad	Member No. 430, x: 52.5 mm
Max. rotation about Y	-0.2	mmrad	FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	-0.2	mmrad	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Method of analysis	Linear		Geometrically linear analysis

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Model: Driepoot-v14

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4.0 RESULTS - SUMMARY

Description	Value	Unit	Comment
Reduction of stiffness			Cross-sections, Members, Surfaces
Number of load increments	1		
Number of iterations	1		
LC5 - Imposed load - multiple acrobats			Deviation 0.00% At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm) At center of gravity of model At center of gravity of model Member No. 1049, x: 157.1 mm Member No. 714, x: 480.0 mm Member No. 765, x: 0.0 mm Member No. 765, x: 0.0 mm Member No. 545, x: 315.0 mm Member No. 765, x: 315.0 mm Member No. 382, x: 46.7 mm Geometrically linear analysis Cross-sections, Members, Surfaces
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	0.00	kN	
Sum of support reactions in Y	0.00	kN	
Sum of loads in Z	-2.40	kN	
Sum of support reactions in Z	-2.40	kN	
Resultant of reactions about X	0.00000	kNm	
Resultant of reactions about Y	0.00000	kNm	
Resultant of reactions about Z	0.00000	kNm	
Max. displacement in X	0.3	mm	
Max. displacement in Y	0.3	mm	
Max. displacement in Z	-1.0	mm	
Max. vector displacement	1.0	mm	
Max. rotation about X	-1.7	mrad	
Max. rotation about Y	-1.7	mrad	
Max. rotation about Z	0.9	mrad	
Method of analysis	Linear		
Reduction of stiffness			
Number of load increments	1		
Number of iterations	1		
LC6 - Imposed load - multiple acrobats +Y swining			Deviation 0.00% At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm) At center of gravity of model At center of gravity of model Member No. 115, x: 338.5 mm Member No. 765, x: 0.0 mm Member No. 678, x: 425.5 mm Member No. 461, x: 265.9 mm Member No. 430, x: 52.5 mm FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm) FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm) Geometrically linear analysis Cross-sections, Members, Surfaces
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	-0.48	kN	
Sum of support reactions in Y	-0.48	kN	
Sum of loads in Z	0.00	kN	
Sum of support reactions in Z	0.00	kN	
Resultant of reactions about X	1.42131	kNm	
Resultant of reactions about Y	0.00000	kNm	
Resultant of reactions about Z	0.00000	kNm	
Max. displacement in X	-0.3	mm	
Max. displacement in Y	-2.0	mm	
Max. displacement in Z	-0.8	mm	
Max. vector displacement	2.1	mm	
Max. rotation about X	-1.2	mrad	
Max. rotation about Y	-0.7	mrad	
Max. rotation about Z	-0.5	mrad	
Method of analysis	Linear		
Reduction of stiffness			
Number of load increments	1		
Number of iterations	1		
LC7 - Wind in +Y			Deviation 0.00% At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm) At center of gravity of model At center of gravity of model Member No. 104, x: 159.6 mm Member No. 686, x: 160.0 mm Member No. 583, x: 84.5 mm Member No. 686, x: 213.4 mm Member No. 744, x: 13.4 mm FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm) FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm) Geometrically linear analysis Cross-sections, Members, Surfaces
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	1.86	kN	
Sum of support reactions in Y	1.86	kN	
Sum of loads in Z	0.00	kN	
Sum of support reactions in Z	0.00	kN	
Resultant of reactions about X	0.07378	kNm	
Resultant of reactions about Y	0.00000	kNm	
Resultant of reactions about Z	-0.00305	kNm	
Max. displacement in X	0.9	mm	
Max. displacement in Y	6.4	mm	
Max. displacement in Z	2.5	mm	
Max. vector displacement	6.8	mm	
Max. rotation about X	-2.3	mrad	
Max. rotation about Y	1.4	mrad	
Max. rotation about Z	1.0	mrad	
Method of analysis	Linear		
Reduction of stiffness			
Number of load increments	1		
Number of iterations	1		
LC8 - Wind in -Y			Deviation 0.00% At center of gravity of model (X:0.00141, Y:-0.00072, Z:4.489E+03 mm) At center of gravity of model At center of gravity of model Member No. 104, x: 159.6 mm Member No. 686, x: 160.0 mm Member No. 583, x: 84.5 mm Member No. 686, x: 213.4 mm Member No. 744, x: 13.4 mm FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm) FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm) Geometrically linear analysis Cross-sections, Members, Surfaces
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	-1.86	kN	
Sum of support reactions in Y	-1.86	kN	
Sum of loads in Z	0.00	kN	
Sum of support reactions in Z	0.00	kN	
Resultant of reactions about X	-0.07524	kNm	
Resultant of reactions about Y	0.00000	kNm	
Resultant of reactions about Z	0.00305	kNm	
Max. displacement in X	-0.9	mm	
Max. displacement in Y	-6.3	mm	
Max. displacement in Z	-2.5	mm	
Max. vector displacement	6.8	mm	
Max. rotation about X	2.3	mrad	
Max. rotation about Y	-1.4	mrad	

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4.0 RESULTS - SUMMARY

Description	Value	Unit	Comment
Max. rotation about Z Method of analysis Reduction of stiffness Number of load increments Number of iterations	-1.0 Linear 1 1	mrad	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm) Geometrically linear analysis Cross-sections, Members, Surfaces
CO1 - Characteristic Values Sum of loads in X Sum of support reactions in X Sum of loads in Y Sum of support reactions in Y Sum of loads in Z Sum of support reactions in Z Resultant of reactions about X Resultant of reactions about Y Resultant of reactions about Z Max. displacement in X Max. displacement in Y Max. displacement in Z Max. vector displacement Max. rotation about X Max. rotation about Y Max. rotation about Z Method of analysis Internal forces referred to deformed system for... Reduction of stiffness Consider favorable effects of tensile forces Divide results by CO factor Number of load increments Number of iterations	 0.00 0.00 0.00 0.00 -2.13 -2.13 0.0 0.0 0.0 0.4 -0.4 -0.2 0.5 0.3 0.3 -0.1 2nd Order <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> 1 3	kN kN kN kN kN kN kNm kNm kNm mm mm mm mm mrad mrad mrad	Deviation 0.00% At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm) At center of gravity of model At center of gravity of model Member No. 117, x: 46.7 mm Member No. 708, x: 46.7 mm Member No. 1035, x: 225.7 mm Member No. 701, x: 143.4 mm FE Node No. 1253 (X: 751.7, Y: -559.2, Z: 7382.5 mm) Member No. 7, x: 200.0 mm FE Node No. 1680 (X: -754.4, Y: -566.3, Z: 7367.7 mm) Second order analysis (Nonlinear, Timoshenko) N, V _y , V _z , M _y , M _z , M _T Materials, Cross-sections, Members, Surfaces
CO2 - Design Internal Forces - 1 acrobat - +Y swing Sum of loads in X Sum of support reactions in X Sum of loads in Y Sum of support reactions in Y Sum of loads in Z Sum of support reactions in Z Resultant of reactions about X Resultant of reactions about Y Resultant of reactions about Z Max. displacement in X Max. displacement in Y Max. displacement in Z Max. vector displacement Max. rotation about X Max. rotation about Y Max. rotation about Z Method of analysis Internal forces referred to deformed system for... Reduction of stiffness Consider favorable effects of tensile forces Divide results by CO factor Number of load increments Number of iterations	 0.00 0.00 0.64 0.64 -6.08 -6.08 -1.9 0.0 0.0 0.5 2.8 -1.5 3.1 3.0 -2.2 1.6 2nd Order <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> 1 3	kN kN kN kN kN kN kNm kNm kNm mm mm mm mm mrad mrad mrad	Deviation 0.00% Deviation 0.00% At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm) At center of gravity of model At center of gravity of model Member No. 119, x: 319.1 mm Member No. 649, x: 50.9 mm Member No. 545, x: 105.0 mm Member No. 765, x: 0.0 mm Member No. 430, x: 262.5 mm Member No. 765, x: 315.0 mm Member No. 372, x: 46.7 mm Second order analysis (Nonlinear, Timoshenko) N, V _y , V _z , M _y , M _z , M _T Materials, Cross-sections, Members, Surfaces
CO3 - Design Internal Forces - 1 acrobat - -Y swing Sum of loads in X Sum of support reactions in X Sum of loads in Y Sum of support reactions in Y Sum of loads in Z Sum of support reactions in Z Resultant of reactions about X Resultant of reactions about Y Resultant of reactions about Z Max. displacement in X Max. displacement in Y Max. displacement in Z Max. vector displacement Max. rotation about X Max. rotation about Y Max. rotation about Z Method of analysis Internal forces referred to deformed system for... Reduction of stiffness Consider favorable effects of tensile forces Divide results by CO factor Number of load increments Number of iterations	 0.00 0.00 -0.64 -0.64 -6.08 -6.08 1.9 0.0 0.0 0.4 -2.7 -1.4 3.0 -3.4 -2.5 1.5 2nd Order <input checked="" type="checkbox"/> <input type="checkbox"/> <input type="checkbox"/> 1 3	kN kN kN kN kN kN kNm kNm kNm mm mm mm mm mrad mrad mrad	Deviation 0.00% Deviation 0.00% At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm) At center of gravity of model At center of gravity of model Member No. 352, x: 177.8 mm Member No. 458, x: 319.1 mm Member No. 430, x: 52.5 mm Member No. 765, x: 0.0 mm Member No. 545, x: 262.5 mm Member No. 765, x: 315.0 mm Member No. 382, x: 46.7 mm Second order analysis (Nonlinear, Timoshenko) N, V _y , V _z , M _y , M _z , M _T Materials, Cross-sections, Members, Surfaces
CO4 - Design Internal Forces - multiple acrobats Sum of loads in X Sum of support reactions in X Sum of loads in Y Sum of support reactions in Y Sum of loads in Z Sum of support reactions in Z	 0.00 0.00 0.32 0.32 -4.48 -4.48	kN kN kN kN kN kN	Deviation 0.00% Deviation 0.00%

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4.0 RESULTS - SUMMARY

Description	Value	Unit	Comment
Resultant of reactions about X	-1.0	kNm	At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm)
Resultant of reactions about Y	0.0	kNm	At center of gravity of model
Resultant of reactions about Z	0.0	kNm	At center of gravity of model
Max. displacement in X	0.5	mm	Member No. 119, x: 425.5 mm
Max. displacement in Y	1.4	mm	Member No. 649, x: 50.9 mm
Max. displacement in Z	-0.8	mm	Member No. 545, x: 105.0 mm
Max. vector displacement	1.5	mm	Member No. 765, x: 0.0 mm
Max. rotation about X	1.5	mrاد	Member No. 430, x: 315.0 mm
Max. rotation about Y	-1.2	mrاد	Member No. 765, x: 315.0 mm
Max. rotation about Z	0.8	mrاد	Member No. 372, x: 46.7 mm
Method of analysis	2nd Order		Second order analysis (Nonlinear, Timoshenko)
Internal forces referred to deformed system for...	<input checked="" type="checkbox"/>		N, V _y , V _z , M _y , M _z , M _T
Reduction of stiffness			Materials, Cross-sections, Members, Surfaces
Consider favorable effects of tensile forces	<input type="checkbox"/>		
Divide results by CO factor	<input type="checkbox"/>		
Number of load increments	1		
Number of iterations	3		
CO5 - internal forces - wind +Y			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	2.24	kN	
Sum of support reactions in Y	2.24	kN	Deviation 0.00%
Sum of loads in Z	-2.88	kN	
Sum of support reactions in Z	-2.88	kN	Deviation 0.00%
Resultant of reactions about X	0.0	kNm	At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm)
Resultant of reactions about Y	0.0	kNm	At center of gravity of model
Resultant of reactions about Z	0.0	kNm	At center of gravity of model
Max. displacement in X	1.6	mm	Member No. 115, x: 338.5 mm
Max. displacement in Y	7.3	mm	Member No. 686, x: 373.4 mm
Max. displacement in Z	2.7	mm	Member No. 581, x: 84.6 mm
Max. vector displacement	7.8	mm	Member No. 686, x: 426.7 mm
Max. rotation about X	2.6	mrاد	FE Node No. 2228 (X: 862.5, Y: -367.1, Z: 7382.5 mm)
Max. rotation about Y	2.0	mrاد	FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	1.1	mrاد	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Method of analysis	2nd Order		Second order analysis (Nonlinear, Timoshenko)
Internal forces referred to deformed system for...	<input checked="" type="checkbox"/>		N, V _y , V _z , M _y , M _z , M _T
Reduction of stiffness			Materials, Cross-sections, Members, Surfaces
Consider favorable effects of tensile forces	<input type="checkbox"/>		
Divide results by CO factor	<input type="checkbox"/>		
Number of load increments	1		
Number of iterations	3		
CO6 - internal forces - wind -Y			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	-2.24	kN	
Sum of support reactions in Y	-2.24	kN	Deviation 0.00%
Sum of loads in Z	-2.88	kN	
Sum of support reactions in Z	-2.88	kN	Deviation 0.00%
Resultant of reactions about X	-0.1	kNm	At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm)
Resultant of reactions about Y	0.0	kNm	At center of gravity of model
Resultant of reactions about Z	0.0	kNm	At center of gravity of model
Max. displacement in X	-0.7	mm	Member No. 75, x: 425.5 mm
Max. displacement in Y	-8.2	mm	Member No. 471, x: 212.7 mm
Max. displacement in Z	-3.3	mm	Member No. 583, x: 56.3 mm
Max. vector displacement	8.8	mm	FE Node No. 691 (X: 119.7, Y: 2274.2, Z: 4951.4 mm)
Max. rotation about X	3.1	mrاد	Member No. 744, x: 13.4 mm
Max. rotation about Y	-1.4	mrاد	FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	-1.3	mrاد	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Method of analysis	2nd Order		Second order analysis (Nonlinear, Timoshenko)
Internal forces referred to deformed system for...	<input checked="" type="checkbox"/>		N, V _y , V _z , M _y , M _z , M _T
Reduction of stiffness			Materials, Cross-sections, Members, Surfaces
Consider favorable effects of tensile forces	<input type="checkbox"/>		
Divide results by CO factor	<input type="checkbox"/>		
Number of load increments	1		
Number of iterations	4		
CO7 - Design Internal Forces - 1 acrobat + wind +Y			
Sum of loads in X	0.00	kN	
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	2.88	kN	
Sum of support reactions in Y	2.88	kN	Deviation 0.00%
Sum of loads in Z	-6.08	kN	
Sum of support reactions in Z	-6.08	kN	Deviation 0.00%
Resultant of reactions about X	-1.9	kNm	At center of gravity of model (X:0.0, Y:0.0, Z:4488.9 mm)
Resultant of reactions about Y	0.0	kNm	At center of gravity of model
Resultant of reactions about Z	0.0	kNm	At center of gravity of model
Max. displacement in X	1.6	mm	Member No. 104, x: 372.3 mm
Max. displacement in Y	10.3	mm	Member No. 686, x: 373.4 mm
Max. displacement in Z	3.8	mm	Member No. 581, x: 56.4 mm
Max. vector displacement	10.9	mm	Member No. 686, x: 426.7 mm
Max. rotation about X	5.0	mrاد	Member No. 430, x: 315.0 mm
Max. rotation about Y	3.3	mrاد	FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	1.7	mrاد	Member No. 372, x: 46.7 mm
Method of analysis	2nd Order		Second order analysis (Nonlinear, Timoshenko)
Internal forces referred to deformed system for...	<input checked="" type="checkbox"/>		N, V _y , V _z , M _y , M _z , M _T
Reduction of stiffness			Materials, Cross-sections, Members, Surfaces

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4.0 RESULTS - SUMMARY

Description	Value	Unit	Comment
Consider favorable effects of tensile forces	<input checked="" type="checkbox"/>		
Divide results by CO factor	<input type="checkbox"/>		
Number of load increments	1		
Number of iterations	4		
CO8 - Design Internal Forces - 1 acrobat + wind -Y			
Sum of loads in X	0.00	kN	Deviation 0.00%
Sum of support reactions in X	0.00	kN	
Sum of loads in Y	-2.88	kN	
Sum of support reactions in Y	-2.88	kN	
Sum of loads in Z	-6.08	kN	
Sum of support reactions in Z	-6.08	kN	
Resultant of reactions about X	1.9	kNm	
Resultant of reactions about Y	0.0	kNm	
Resultant of reactions about Z	0.0	kNm	
Max. displacement in X	-1.5	mm	
Max. displacement in Y	-10.3	mm	Member No. 465, x: 225.7 mm
Max. displacement in Z	-4.2	mm	Member No. 581, x: 84.6 mm
Max. vector displacement	11.1	mm	Member No. 466, x: 106.4 mm
Max. rotation about X	-5.3	mrاد	Member No. 545, x: 262.5 mm
Max. rotation about Y	2.5	mrاد	FE Node No. 2808 (X: -868.7, Y: -356.4, Z: 7382.5 mm)
Max. rotation about Z	-2.2	mrاد	FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Method of analysis	2nd Order		Second order analysis (Nonlinear, Timoshenko)
Internal forces referred to deformed system for...	<input checked="" type="checkbox"/>		N, V _y , V _z , M _y , M _z , M _T
Reduction of stiffness			Materials, Cross-sections, Members, Surfaces
Consider favorable effects of tensile forces	<input checked="" type="checkbox"/>		
Divide results by CO factor	<input type="checkbox"/>		
Number of load increments	1		
Number of iterations	3		
Summary			
Max. displacement in X	1.6	mm	CO5, Member No. 115, x: 338.5 mm
Max. displacement in Y	-10.3	mm	CO8, Member No. 465, x: 225.7 mm
Max. displacement in Z	-4.2	mm	CO8, Member No. 581, x: 84.6 mm
Max. vector displacement	11.1	mm	CO8, Member No. 466, x: 106.4 mm
Max. rotation about X	-5.3	mrاد	CO8, Member No. 545, x: 262.5 mm
Max. rotation about Y	3.3	mrاد	CO7, FE Node No. 1384 (X: 113.6, Y: 930.5, Z: 7382.5 mm)
Max. rotation about Z	-2.2	mrاد	CO8, FE Node No. 2817 (X: -873.9, Y: -359.3, Z: 7367.7 mm)
Other Settings			
Number of 1D finite elements			: 1318
Number of 2D finite elements			: 3937
Number of 3D finite elements			: 8065
Number of FE mesh nodes			: 5050
Number of equations			: 30300
Max. number of iterations			: 20
Number of divisions for member results			: 10
Division of cable/foundation/tapered members			: 10
Number of member divisions for searching maximum values			: 10
Subdivisions of FE mesh for graphical results			: 0
Percentage of iterations according to Picard method in combination with Newton-Raphson method			: 5 %
Options			
<input checked="" type="checkbox"/> Activate shear stiffness of members (Ay, Az)			
<input checked="" type="checkbox"/> Activate member divisions for large deformation or post-critical analysis			
<input checked="" type="checkbox"/> Activate entered stiffness modifications			
<input type="checkbox"/> Ignore rotational degrees of freedom			
<input checked="" type="checkbox"/> Check of critical forces of members			
<input type="checkbox"/> Nonsymmetric direct solver if demanded by nonlinear model			
Method for the system of equations			<input type="radio"/> Direct <input type="radio"/> Iteration <input checked="" type="radio"/> Mindlin <input type="radio"/> Kirchhoff
Plate bending theory			<input type="radio"/> 32-bit <input checked="" type="radio"/> 64-bit
Solver version			
Precision and Tolerance			
<input type="checkbox"/> Change default setting			

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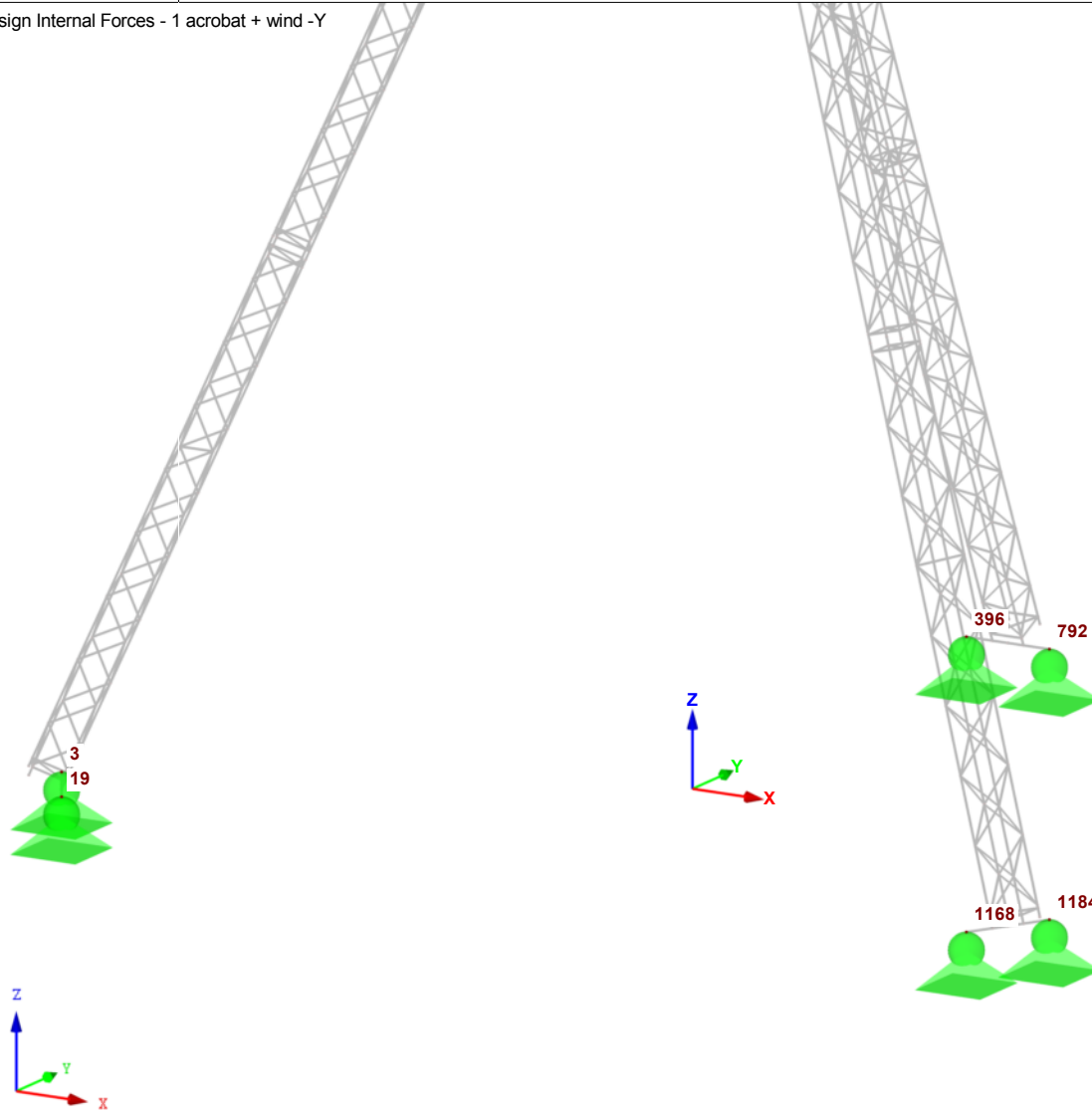
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MODEL - NODE NUMBERS WITH SUPPORT

CO8: Design Internal Forces - 1 acrobat + wind -Y

Isometric



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■ 4.1 NODES - SUPPORT FORCES

Node No.	LC/CO	Support Forces [kN]			Support Moments [kNm]			Comment
		P _x	P _y	P _z	M _x	M _y	M _z	
3	CO1	-0.10	-0.01	-0.36	0.00	0.00	-0.01	
	CO2	-0.46	-0.11	-1.15	0.00	0.00	-0.05	
	CO3	-0.28	-0.06	-0.88	0.00	0.00	-0.04	
	CO4	-0.30	-0.07	-0.81	0.00	0.00	-0.03	
	CO5	-0.60	-0.05	-1.40	0.00	0.00	-0.04	
	CO6	0.32	0.01	0.44	0.00	0.00	0.01	
	CO7	-0.92	-0.14	-2.06	0.00	0.00	-0.07	
	CO8	0.17	-0.03	0.03	0.00	0.00	-0.02	
19	CO1	-0.06	-0.08	-0.35	0.00	0.00	0.01	
	CO2	-0.05	-0.10	-0.53	0.00	0.00	0.02	
	CO3	-0.46	-0.45	-1.49	0.00	0.00	0.07	
	CO4	-0.07	-0.11	-0.50	0.00	0.00	0.02	
	CO5	0.58	0.56	1.12	0.00	0.00	-0.08	
	CO6	-0.75	-0.77	-2.07	0.00	0.00	0.11	
	CO7	0.61	0.57	1.06	0.00	0.00	-0.07	
	CO8	-1.12	-1.11	-3.08	0.00	0.00	0.16	
396	CO1	-0.04	0.09	-0.35	0.00	0.00	0.01	
	CO2	-0.15	0.53	-1.36	0.00	0.00	0.07	
	CO3	-0.07	0.18	-0.66	0.00	0.00	0.02	
	CO4	-0.10	0.33	-0.92	0.00	0.00	0.04	
	CO5	-0.13	0.61	-1.16	0.00	0.00	0.08	
	CO6	0.03	-0.36	0.20	0.00	0.00	-0.05	
	CO7	-0.23	1.02	-2.04	0.00	0.00	0.13	
	CO8	0.01	-0.30	0.02	0.00	0.00	-0.04	
792	CO1	0.04	0.10	-0.36	0.00	0.00	-0.01	
	CO2	0.15	0.54	-1.36	0.00	0.00	-0.07	
	CO3	0.07	0.19	-0.67	0.00	0.00	-0.02	
	CO4	0.10	0.33	-0.92	0.00	0.00	-0.04	
	CO5	0.13	0.61	-1.16	0.00	0.00	-0.08	
	CO6	-0.03	-0.35	0.19	0.00	0.00	0.05	
	CO7	0.23	1.02	-2.04	0.00	0.00	-0.13	
	CO8	0.00	-0.30	0.01	0.00	0.00	0.04	
1168	CO1	0.06	-0.08	-0.36	0.00	0.00	-0.01	
	CO2	0.06	-0.10	-0.53	0.00	0.00	-0.02	
	CO3	0.46	-0.46	-1.50	0.00	0.00	-0.07	
	CO4	0.07	-0.10	-0.51	0.00	0.00	-0.02	
	CO5	-0.56	0.59	1.11	0.00	0.00	0.07	
	CO6	0.73	-0.81	-2.07	0.00	0.00	-0.11	
	CO7	-0.59	0.60	1.05	0.00	0.00	0.07	
	CO8	1.10	-1.15	-3.08	0.00	0.00	-0.16	
1184	CO1	0.10	-0.01	-0.35	0.00	0.00	0.01	
	CO2	0.45	-0.12	-1.14	0.00	0.00	0.05	
	CO3	0.29	-0.05	-0.88	0.00	0.00	0.04	
	CO4	0.29	-0.07	-0.81	0.00	0.00	0.03	
	CO5	0.58	-0.08	-1.39	0.00	0.00	0.04	
	CO6	-0.31	0.04	0.44	0.00	0.00	-0.01	
	CO7	0.89	-0.18	-2.05	0.00	0.00	0.08	
	CO8	-0.15	0.01	0.03	0.00	0.00	0.02	

Project: 2016-driepoot

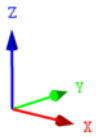
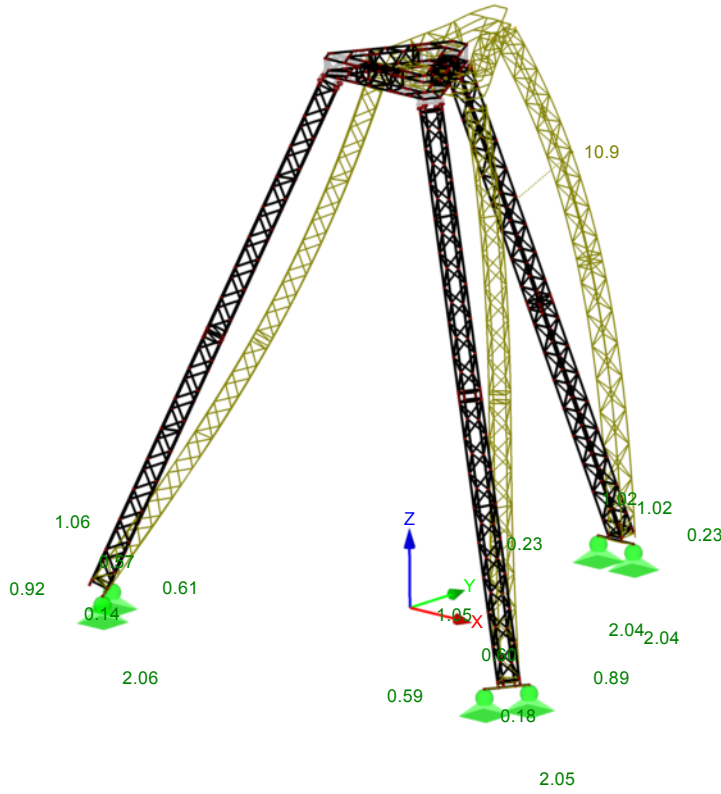
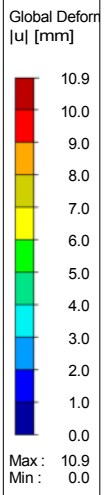
Model: Driepoot-v14

Date: 18-07-16

GLOBAL DEFORMATIONS U, SUPPORT REACTIONS - ACROBAT AND WIND IN +Y

CO7: Design Internal Forces - 1 acrobat + wind +Y
 Global Deformations u
 Support Reactions[kN]

Isometric



Max P-Z: 1.06, Min P-Z: -2.06 kN
 Max P-Y: 1.02, Min P-Y: -0.18 kN
 Max P-X: 0.89, Min P-X: -0.92 kN
 Max u: 10.9, Min u: 0.0 mm
 Factor of deformations: 110.00

Project: 2016-driepoot

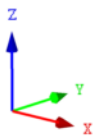
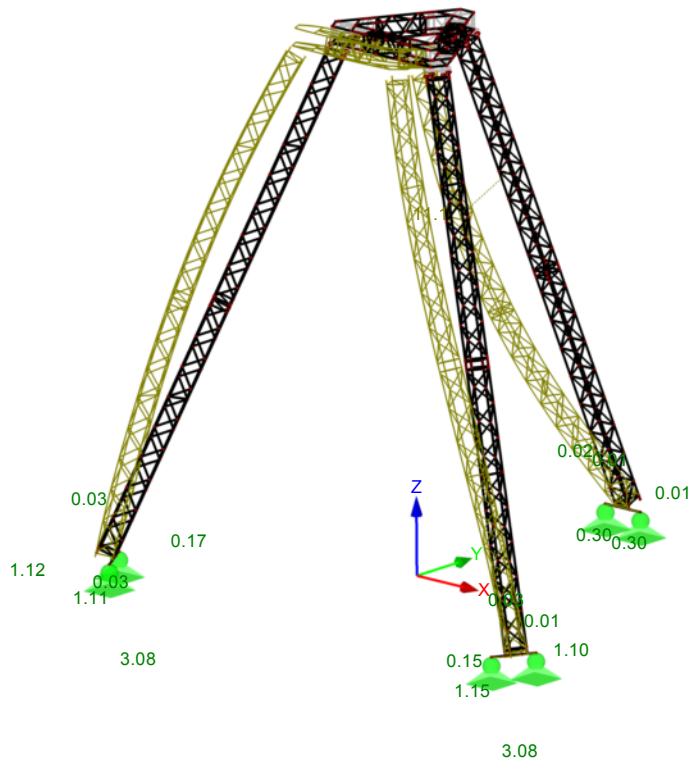
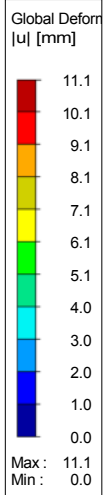
Model: Driepoot-v14

Date: 18-07-16

GLOBAL DEFORMATIONS U, SUPPORT REACTIONS - ACROBAT AND WIND IN -Y

CO8: Design Internal Forces - 1 acrobat + wind -Y
 Global Deformations u
 Support Reactions[kN]

Isometric



Max P-Z: 0.03, Min P-Z: -3.08 kN
 Max P-Y: 0.01, Min P-Y: -1.15 kN
 Max P-X: 1.10, Min P-X: -1.12 kN
 Max u: 11.1, Min u: 0.0 mm
 Factor of deformations: 100.00

Project: 2016-driepoot

Model: Driepoot-v14

Date: 18-07-16

■ 4.1 NODES - SUPPORT FORCES - RC1

Result Combinations

Node No.	RC		Support Forces [kN]			Support Moments [kNm]			Comment
			P _x	P _y	P _z	M _x	M _y	M _z	
3	RC1	Max	0.32	0.01	0.44	0.00	0.00	0.01	
		Min	-0.92	-0.14	-2.06	0.00	0.00	-0.07	
19	RC1	Max	0.61	0.57	1.12	0.00	0.00	-0.16	
		Min	-1.12	-1.11	-3.08	0.00	0.00	-0.08	
396	RC1	Max	0.03	1.02	0.20	0.00	0.00	0.13	
		Min	-0.23	-0.36	-2.04	0.00	0.00	-0.05	
792	RC1	Max	0.23	1.02	0.19	0.00	0.00	0.05	
		Min	-0.03	-0.35	-2.04	0.00	0.00	-0.13	
1168	RC1	Max	1.10	0.60	1.11	0.00	0.00	0.07	
		Min	-0.59	-1.15	-3.08	0.00	0.00	-0.16	
1184	RC1	Max	0.89	0.04	0.44	0.00	0.00	0.08	
		Min	-0.31	-0.18	-2.05	0.00	0.00	-0.01	

Project: 2016-driepoot

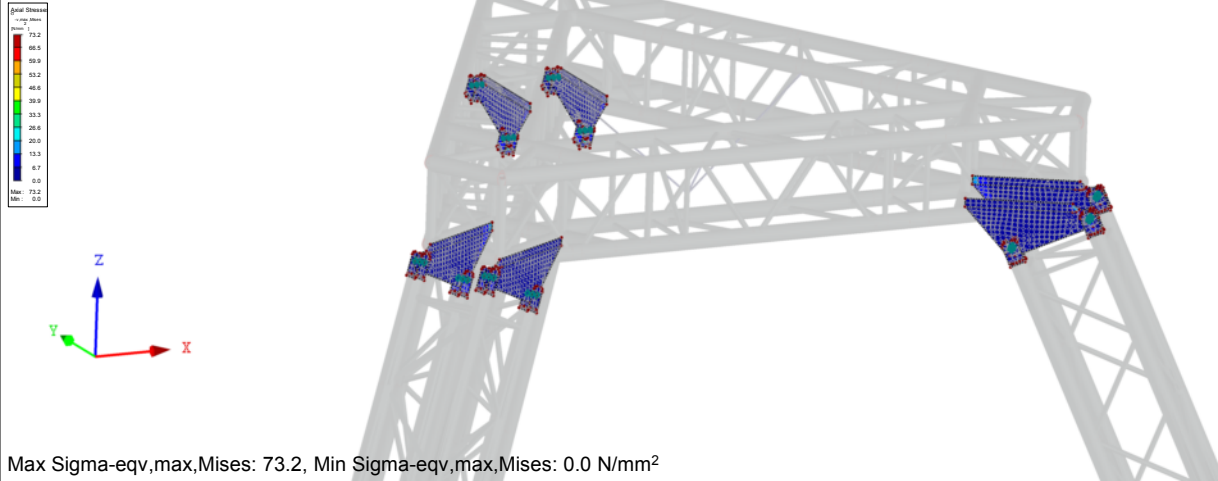
Model: Driepoot-v14

Date: 18-07-16

AXIAL STRESSES $\sigma_{eqv,Max,Mises}$ IN THE SURFACES CONNECTING THE TOPBLOCK AND THE LEGS

RC1: Design Internal Forces
 Surfaces Stresses Sigma-eqv,max,Mises
 Result Combinations: Max and Min Values

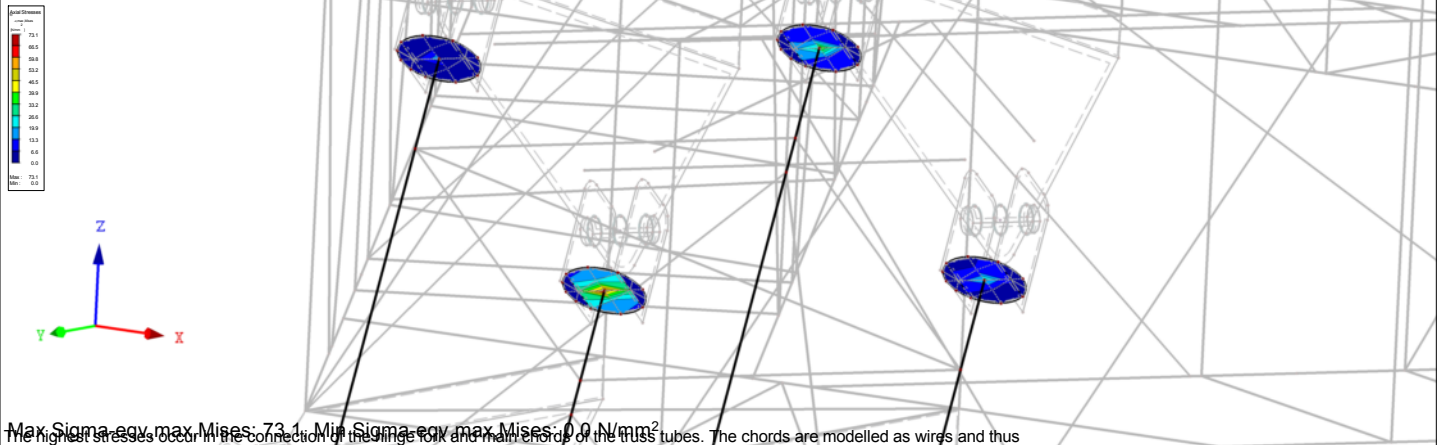
Isometric



AXIAL STRESSES $\sigma_{eqv,Max,Mises}$ IN THE SURFACES CONNECTING THE TRUSS CHORDS AND HINGES

RC1: Design Internal Forces
 Surfaces Stresses Sigma-eqv,max,Mises
 Result Combinations: Max and Min Values

Isometric



The highest stresses occur in the connection of the hinge fork and main chords of the truss tubes. The chords are modelled as wires and thus show high point-like stress. It's more useful to analyse this connection in the RF_STEEL module: in fact the hinge is welded like a conical coupler all around the end of the tube: if stresses remain below HAZ numbers, the connection is sufficiently strong.

Project: 2016-driepoot Model: Driepoot-v14 Date: 18-07-16

RF-STEEL Members
CA1
General stress analysis
of steel members

1.1.1 GENERAL DATA

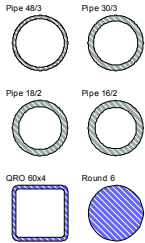
Members to design:	All	
Load combinations to design:	CO7	Design Internal Forces - 1 acrobat + wind +Y
	CO8	Design Internal Forces - 1 acrobat + wind -Y

In order to have a proper indication of failure, the yield values in the Heat Affected Zone are modelled

1.2 MATERIALS

Matl. No.	Material Description	Safety Factor γ_M [-]	Yield Strength f_{yk} [N/mm ²]	Limit Stresses [N/mm ²]			
				Manually	Limit σ_x	Limit τ	Limit σ_{eqv}
1	Aluminium EN-AW 6082 T6/T651*	1.10	100.000	<input type="checkbox"/>	90.909	52.486	90.909
2	HDT1200M 1.0965	1.00	900.000	<input type="checkbox"/>	900.000	519.615	900.000
3	Steel S 235 JR	1.00	235.000	<input type="checkbox"/>	235.000	135.677	235.000

1.3.1 CROSS-SECTIONS



Sect. No.	Matl. No.	Cross-section Description	I_x [cm ⁴] A [cm ²]	I_y [cm ⁴] $\alpha_{pl,y}$	I_z [cm ⁴] $\alpha_{pl,z}$	Comment
1	1	Pipe 48/3	21.57	10.78	10.78	
			4.24	1.35	1.35	
2	1	Pipe 30/3	4.69	2.35	2.35	
			2.54	1.40	1.40	
3	1	Pipe 18/2	0.65	0.33	0.33	
			1.01	1.42	1.42	
4	1	Pipe 16/2	0.44	0.22	0.22	
			0.88	1.44	1.44	
5	3	QRO 60x4 EN 10210-2:2006	72.50	45.40	45.40	
			8.79	1.21	1.21	
6	2	Round 6	0.01	0.01	0.01	
			0.28	1.70	1.70	

RF-STEEL Members
CA1
General stress analysis
of steel members

2.1 STRESSES BY CROSS-SECTION

Sect. No.	Member No.	Location x [mm]	S-Point No.	Load Case	Stress Type	Stress [N/mm ²]		Stress Ratio
						Existing	Limit	
1	Pipe 48/3							
	399	0.0	3	CO8	Sigma Total	-32.703	90.909	0.36
	317	38.9	10	CO7	Tau Total	-14.303	52.486	0.27
	399	0.0	3	CO8	Sigma-eqv	32.849	90.909	0.36
2	Pipe 30/3							
	876	0.0	35	CO8	Sigma Total	-20.724	90.909	0.23
	854	238.9	30	CO7	Tau Total	-1.762	52.486	0.03
	876	0.0	35	CO8	Sigma-eqv	20.732	90.909	0.23
3	Pipe 18/2							
	367	0.0	2	CO7	Sigma Total	28.081	90.909	0.31
	410	0.0	11	CO8	Tau Total	2.039	52.486	0.04
	367	0.0	2	CO7	Sigma-eqv	28.093	90.909	0.31
4	Pipe 16/2							
	363	0.0	25	CO8	Sigma Total	30.811	90.909	0.34
	353	143.4	36	CO8	Tau Total	-1.728	52.486	0.03
	363	0.0	25	CO8	Sigma-eqv	30.824	90.909	0.34
5	QRO 60x4 EN 10210-2:2006							
	1155	0.0	1	CO8	Sigma Total	-47.696	235.000	0.20
	1155	200.0	4	CO8	Tau Total	8.526	135.677	0.06
	1155	0.0	1	CO8	Sigma-eqv	48.585	235.000	0.21
6	Round 6							
	545	0.0	10	CO7	Sigma Total	104.315	900.000	0.12
	545	0.0	37	CO7	Tau Total	0.354	519.615	0.00
	545	0.0	10	CO7	Sigma-eqv	104.317	900.000	0.12

CO5 Wind in +Y direction										
Support Forces [kN]				<i>should be negat</i>				<i>orientation</i>	<i>fric ion coeff</i>	<i>ballast</i>
0,6										
Node	P _{X'}	P _{Y'}	P _{Z'}	P _{X'} per leg	P _{Y'} per leg	P _{hor'} per leg	P _{Z'} per leg		Ffrict : Phor	kg
3	-0,60	-0,05	-1,40	-0,02	0,51	0,510	-0,28	-X -Y leg	0,33	222
19	0,58	0,56	1,12							
396	-0,13	0,61	-1,16	0,00	1,22	1,220	-2,32	+Y leg	1,14	
792	0,13	0,61	-1,16							
1168	-0,56	0,59	1,11	0,02	0,51	0,510	-0,28	+X -Y leg	0,33	222
1184	0,58	-0,08	-1,39							
Σ Loads	-0,00	2,24	-2,88				-2,88			
CO6 Wind in -Y direction										
Support Forces [kN]										
Node	P _{X'}	P _{Y'}	P _{Z'}	P _{X'} per leg	P _{Y'} per leg	P _{hor'} per leg	P _{Z'} per leg			
3	0,32	0,01	0,44	-0,43	-0,76	0,873	-1,63	-X -Y leg	1,12	
19	-0,75	-0,77	-2,07							
396	0,03	-0,36	0,20	0,00	-0,71	0,710	0,39	+Y leg	-0,33	112
792	-0,03	-0,35	0,19							
1168	0,73	-0,81	-2,07	0,42	-0,77	0,877	-1,63	+X -Y leg	1,12	
1184	-0,31	0,04	0,44							
Σ Loads	-0,01	-2,24	-2,87				-2,87			
CO7 Wind and acrobat in +Y direction										
Support Forces [kN]										
Node	P _{X'}	P _{Y'}	P _{Z'}	P _{X'} per leg	P _{Y'} per leg	P _{hor'} per leg	P _{Z'} per leg			
3	-0,92	-0,14	-2,06	-0,31	0,43	0,530	-1,00	-X -Y leg	1,13	
19	0,61	0,57	1,06							
396	-0,23	1,02	-2,04	0,00	2,04	2,040	-4,08	+Y leg	1,20	
792	0,23	1,02	-2,04							
1168	-0,59	0,60	1,05	0,30	0,42	0,516	-1,00	+X -Y leg	1,16	
1184	0,89	-0,18	-2,05							
Σ Loads	-0,01	2,89	-6,08				-6,08			
CO8 Wind and acrobat in -Y direction										
Support Forces [kN]										
Node	P _{X'}	P _{Y'}	P _{Z'}	P _{X'} per leg	P _{Y'} per leg	P _{hor'} per leg	P _{Z'} per leg			
3	0,17	-0,03	0,03	-0,95	-1,14	1,484	-3,05	-X -Y leg	1,23	
19	-1,12	-1,11	-3,08							
396	0,01	-0,30	0,02	0,01	-0,60	0,600	0,03	+Y leg	-0,03	162
792	0,00	-0,30	0,01							
1168	1,10	-1,15	-3,08	0,95	-1,14	1,484	-3,05	+X -Y leg	1,23	
1184	-0,15	0,01	0,03							
Σ Loads	0,01	-2,88	-6,07				-6,07			